National Library of Canada

Bibliothèque nationale du Canada

Canadian Theses Service

Services des thèses canadiennes

Ottawa, Canada K1A 0N4

CANADIAN THESES

THÈSES CANADIENNES

NOTICE

The quality of this microfiche is heavily dependent upon the quality of the original thesis submitted for microfilming. Every effort has been made to ensure the highest quality of reproduction possible.

If pages are missing, contact the university which granted the degree.

Some pages may have indistinct print especially if the original pages were typed with a poor typewriter ribbon or if the university sent us an inferior photocopy.

Previously copyrighted materials (journal articles, published tests, etc.) are not filmed.

Reproduction in full or in part of this film is governed by the Canadian Copyright Act, R.S.C. 1970, c. C-30.

AVIS

La qualité de cette microfiche dépend grandement de la qualité de la thèse soumise au microfilmage. Nous avons tout fait pour assurer une qualité supérieure de reproduction.

S'il manque des pages, veuillez communiquer avec l'université qui a conféré le grade.

La qualité d'impression de certaines pages peut laisser à désirer, surtout si les pages originales ont été dactylographiées à l'aide d'un ruban usé ou si l'université nous a fait parvenir une photocopie de qualité inférieure.

Les documents qui font déjà l'objet d'un droit d'auteur (articles de revue, examens publiés, etc.) ne sont pas microfilmés.

La reproduction, même partielle, de ce microfilm est soumise à la Loi canadienne sur le droit d'auteur, SRC 1970, c. C-30.

THIS DISSERTATION
HAS BEEN MICROFILMED
EXACTLY AS RECEIVED

LA THÈSE A ÉTÉ MICROFILMÉE TELLE QUE NOUS L'AVONS REÇUE



REGRESSION ANALYSIS PROCEDURES WITH HIGHER ORDER MOVING AVERAGE ERRORS

by

Askar Hassan Choudhury

B. Sc. (Hons.), Jahangirnagar University, 1974M. Sc., Jahangirnagar University, 1975

A THESIS SUBMITTED IN PARTIAL FULFILLMENT OF

THE REQUIREMENTS FOR THE DEGREE OF

MASTER OF SCIENCE

in the Department

o.f

Mathematics and Statistics

SIMON FRASER UNIVERSITY

July, 1985

All rights reserved. This thesis may not be reproduced in whole or in part, by photocopy or other means, without permission of the author.

Permission has been granted to the National Library of Canada to microfilm this thesis and to lend or sell copies of the film.

The author (copyright owner) has reserved other publication rights, and neither the thesis nor extensive extracts from it may be printed or otherwise reproduced without his/her written permission.

L'autorisation a été accordée à la Bibliothèque nationale du Canada de microfilmer cette thèse et de prêter ou de vendre des exemplaires du film.

L'auteur (titulaire du droit d'auteur) se réserve les autres droits de publication; ni la thèse ni de longs extraits de celle-ci ne doivent être imprimés ou autrement reproduits sans son autorisation écrite.

ISBN 0-315-30800-1

APPROVAL

Askar Choudhury Name: Master of Science Degree: Regression Analysis Procedures with Higher Order Title of Thesis: Moving Average Errors. Examining Committee: Chairman: A.R. Freedman D.M. Eaves Senior Supervisor R.A. Lockhart C. Villegas K.L. Weldon External Examiner

Date approved: __July 12, 1985

PARTIAL COPYRIGHT LICENSE

I hereby grant to Simon Fraser University the right to lend my thesis, project or extended essay (the title of which is shown below) to users of the Simon Fraser University Library, and to make partial or single copies only for such users or in response to a request from the library of any other university, or other educational institution, on its own behalf or for one of its users. I further agree that permission for multiple copying of this work for scholarly purposes may be granted by me or the Dean of Graduate Studies. It is understood that copying or publication of this work for financial gain shall not be allowed without my written permission.

Title of Thesis/Project/Extended Essay

October 28, 1985.

(date)

REGRI	ESSION ANALYSI	S PROCED	URES WITH	HIGHER C	RDER	
MOVIN	NG AVERAGE ER&	ORS.		į.		
	**				est High	
	ν					
Author:		6			,	,
	(signature) Askar Hassan	Choudhu	ry			5
4	(nama) å			.3	14	

ABSTRACT

REGRESSION ANALYSIS PROCEDURES WITH HIGHER ORDER MOVING AVERAGE ERRORS

An easily implemented exact transformation is presented to transform the generalized regression problem with moving average errors; the transformed variables are used in Generalized Least Squares and Maximum Likelihood estimation. The MacDonald and MacKinnon Procedure is extended for higher order moving average process from the first order. A simulation experiment is conducted to observe the performance of three different procedures; a) General Procedure b) MacDonald & MacKinnon Procedure c) Phillips Procedure. In small samples, it is suggested that the General Procedure performs better. An efficient way to obtain the exact 'covariance determinant occurring in the likelihood function is presented. An extension to higher order of Park and Heikes's Modified Approximate (MAPX) transformation for first order moving average process is derived. The relative efficiency of the regression coefficient estimate using this transformation to that using the exact(GLS) transformation and also to Ordinary Least Squares(OLS) is obtained numerically. The results suggested that MAPX performs as well as the exact transformation for a certain range of moving average parameters, depending on the sample size.

Dedication

To my dear "Abba and Amma."

Acknowledgements

I would like to thank Dr. David Eaves, my senior supervisor, for his scholarly guidance and patient encouragement during the preparation of this thesis. Thanks are also due to Professor C. E. Villegas and Dr. R. Lockhart for their advice. Professors P. Kennedy, D. Maki, and R. A. Holmes of Economics, Dr. S. Kloster of Computing Centre, and Betty Dwyer of Mathematics & Statistics, of Simon Fraser University, for their constant cooperation throughout my research. Kathy Hammes and Sylvia Holmes were a great help to me.

The Statistics Division of the Government of Bangladesh and its scholarly Secretary Dr. A. K. M. Ghulam Rabbani provided me necessary leave and administrative support during my study at Simon Fraser University. Professors K. S. Ahmed, M. Kabir, K. C. Bhuyan, A. Sufian, A. Sobhan and M. M. Ahamed of Jahangirnagar University were always supportive to me. I am indebted to all of them.

TABLE OF CONTENTS

Approval	,	(ii	i.)
Abstract		"(ii	ίi
Dedication		(iv	₇)
Acknowledgements		(v))
Table of Contents	% • ·	(vi	i)
Chapter 1: Introduction		<u> </u>	
Chapter 2: Exact Estimator for the Higher Or Moving Average Process in Regress Errors 2.1 General Problem		4 5	•
2.2 Box-Jenkins Approach	1904 je	6	
2.2.1 Stationarity		6	
2.2.2 Test for Stationarity	#. 	8	
2.2.3 Stationarity Condition	10 gr	B	,
2.2.4 Invertibility Condition	.	9	
2.3 Model Building Strategy		10	
2.3.1 Identification Problem		10,	-
2.3.2 Estimation Problem		15	. 1
2.3.3 Diagnostic Checking	• ,	18	13
2.4 Regression Equation with Movi	ng .	20	
2.4.1 Regression Model	`.,	21	

			Tr. The	
2.5		rent Prod formation	cedures for	24
			· ·	1
	2.5.1	General	Procedure	25
	, « t	2.5.1.1	Transformation Matrix	26
·.		2.5.1.2	Transformation in Recursive Form	27
	2,.5.2	MacDonal Procedut		30
	2.5.3	Phillips	Procedure	33
2.6	Method	of Esti	mation	36
	2.6.1	General	Procedure	36
_		2.6.1.1	Estimated Generalized Least Square	36
		2.6.1.2	Maximum Likelihood	3.7
	2.6.2	MacDonal Procedur		38
		/	Estimated Generalized Least Square	38
		2.6.2.2	Maximum Likelihood	38
	2.6.3	Phillips	Procedure	39
•			Estimated Generalized Least Square	39
		2.6.3.2	Maximum Likelihood	39

	2.7 Simulation Experiment	4,0
-	2.8 Empirical Results	41
	2.9 Specification Error	5 0
Chapter 3:	Exact Determinant of Covariance Matrix	53
	3.1 Determinant of Covariance Matrix Ω^{\prime}	54
	3 2 Determinant from the Transformation of General Procedure	54
~ ,	3.3 Exact Determinant using Θ Matrix	55
Chapter 4:	Approximate Estimator for the Higher Order Moving Average Process in Regression Errors	62
	4.1 Approximate Transformations for MA process	63
. "	4.2 Modified Approximate Transformation (MAPX) for Higher Order MA process	69
	4.3 Empirical Results	73
Chapter 5:	Conclusion	7.7
Appendix A.		81
Appendix B.		89
Appendix C.		95
Appendix E.		97
Appendix F.	1	03
Appendix G.	1	09
Appendix H.	1	15
Bibliography	y ,	17

CHAPTER 1

INTRODUCTION

This thesis reports on the generalized regression problem, with moving average errors and the estimation of regression coefficients in the presence of higher order moving average errors.

In Chapter 2 an easily implemented exact transformation procedure is suggested, which can be used for both GLS and Maximum Likelihood. A simulation experiment which demonstrates the effectiveness of the suggested transformation procedure called General Procedure (GNL) is presented. Another procedure suggested by MacDonald and MacKinnon(MM) (1985) is extended for higher order moving average process. The simulation experiment conducted includes three different transformation procedures, a)General procedure(GNL), b)MacDonald and MacKinnon Procedure(MM) and c)Phillips Procedure(PHL). We also discuss the Univariate Time Series analysis (Box-Jenkins approach), which we have used in our regression error process.

For Maximum Likelihood the determinant can be obtained as a by-product of GNL procedure, while this is not possible for the other two procedures (discussed in Chapter 2). In Chapter 3 we also have suggested an efficient and simple way to obtain the exact determinant for the covariance matrix, which can be used in the Maximum Likelihood estimation for all three procedures, specifically for MM and PHL.

While exact transformation needs much more effort than the approximate transformation, for large samples approximate transformations can be used instead of exact transformations. In Chapter 4 we have discussed various kinds of transformation for 1st order moving average process. We have extended the Modified Approximate transformation (MAPX) procedure, to apply to higher order moving average processes, suggested by Park and Heikes, (1983). We have computed numerically the relative efficiencies of MAPX to GLS and OLS to see its effectiveness for a certain range of moving average parameters.

CHAPTER 2

EXACT ESTIMATOR FOR THE HIGHER ORDER MOVING AVERAGE PROCESS IN REGRESSION ERRORS

2.1 General Problem

It has become an increasing practice to use 'Univariate Time Series' analysis combined with 'Econometric' problems. In our conventional regression model, sometimes called Ordinary Least Squares (OLS), one of the assumptions about regression error is that, the variance-covariance matrix is $\sigma^2 I_n$, which implies that the error variance is homoscedastic and there are no correlations between the errors themselves. But problems arise when this assumption breaks down, e.g., if the homoscedastic property remain and the other one breaks down, which usually happens in Time Series problems. We then have a covariance matrix of regression error of the form $\sigma^2 \Omega$, where Ω is assumed to be known or at least could be estimated. If Ω is known then we can perform the Generalized Least Squares (GLS) which has the same properties as OLS.

In practice Ω is unknown and some kind of restrictive assumptions are made about its structure and since we have to estimate Ω (where estimated Ω will be denoted as V), we would no longer have the properties of GLS. This would lead us to the Estimated Generalized Least Square (EGLS) method. Like GLS, EGLS is also performed in two stages, using OLS in both the stages, only with the exception that estimated values of the parameters are used instead of true value of the parameters. Since it is not, in general, an easy task to find the finite sample properties of EGLS estimators, we can use the Monte Carlo

experiment and since it is, by its nature, model specific and also depends on data sets, the findings can not be generalized, but we will have some insights about the efficiencies of the EGLS estimators. When a specific assumption about the distribution of the regression error is made, the Maximum Likelihood (ML) method of estimation becomes an alternative to EGLS and the parameters are estimated by maximizing the likelihood function.

2.2 Box-Jenkins Approach

If the above mentioned problem arises, i.e., if Ω is not a *- diagonal matrix, we have to classify the error generating process and it can be done by using Box-Jenkins approach. We will restrict our discussion to the stationary process, since, given stationarity, any series can be well-approximated by either a moving average, autoregressive or mixture of both (see Granger, 1980, p.60).

2.2.1 Stationarity

One of our assumptions is that the underlying stochastic process, in our case the regression error vector, is stationary. If the covariance characteristics of the stochastic process change over time, the process is nonstationary; on the other hand, if it is fixed it is stationary. A stationary stochastic process can be classified into,

- a) Strictly Stationary
- b) Weakly Stationary

a) Strictly Stationary Process:

A process is said to be strictly stationary if its distributional properties are unaffected by change of time origin, i.e., if the joint probality distribution of the observations, say u_{t1} u_{t2} u_{tn} at a set of different time points $t1, t2, \ldots, tn$ is invariant with respect to displacement of time.

b) Weakly Stationary Process:

A stochastic process is said to be weakly stationary if the moments up to some order k depends only on time differences but not on time origin. Therefore, if the series (process) is stationary with respect to mean and covariance, we call it weakly stationary of second order. This kind of weak stationary along with normality assumption makes it strictly stationary (see Box and Jenkins, 1970, p.30).

2.2.2 Test for Stationarity

Therefore, before proceeding to data analysis we need to check whether the data to be analysed are stationary or not.

Box-Jenkins and others suggested plotting the observations against time and looking whether there is any evident trend in mean or trend in variance, and also plotting the autocorrelation function (ACF). If the ACF for different lags does not die out quickly, i.e., if they are almost 1, then it is an indication that the process is nonstationary; otherwise, it is stationary. Recently, an approach to stationarity testing has been given by Ali and Thalheimar (1983, pp.249-257). Basically, they developed four test-statistics for four different distributions: normal, logistic, double exponential, and Cauchy. They showed if the test-statistics are insignificant then the series may be considered stationary. This method is not widely practiced, which may be due to unavailability of the program.

2.2.3 Stationarity Condition

If an AR(p) process,

$$u_{t} = \phi_{1}u_{t-1} + \phi_{2}u_{t-2} + \cdots + \phi_{p}u_{t-p} + \epsilon_{t}$$
or, $(1 - \phi_{1}\beta - \phi_{2}\beta^{2} - \cdots - \phi_{p}\beta^{p})u_{t} = \phi(\beta)u_{t} = \epsilon_{t}$

is to be stationary, it must satisfy the condition that roots of the characteristic equation (Box and Jenkins, 1976,pp.53-54)

$$\phi(\beta) = 0 \tag{2.1}$$

should lie outside the unit circle,

i.e., the solutions β_1 , β_2 ,, β_p to eqn. (2.1) must all be greater than 1 in magnitude. Specifically, for AR(1) process, the equation (2.1) becomes,

$$1 - \phi_1 \beta = 0.$$

So that the solution should satisfy,

$$|\beta| = \frac{1}{|\phi_1|} > 1$$

which implies that, $|\phi_1| < 1$.

2.2.4 Invertibility Condition ,

Analogous to the stationarity condition for autoregressive process, if an MA(q) process,

$$u_t = \epsilon_t - \theta_1 \epsilon_{t-1} - \theta_2 \epsilon_{t-2} - \cdots - \theta_q \epsilon_{t-q}$$

is to be invertible, it must satisfy the condition, that the roots of the characteristic equation,

$$\theta(\beta) = 1 - \theta_1 \beta - \theta_2 \beta^2 - \dots - \theta_q \beta^q = 0$$
 (2.2)

must lie outside the unit circle,

i.e., the solutions β_1 , β_2 ,, β_q to eqn. (2.2) must all be greater than one (see Box-Jenkins,1976, pp. 50-51).

For MA(1) process,

$$1 - \theta_1 \beta = 0$$

Therefore,

$$|\beta| = \frac{1}{|\theta_1|} > 1$$

which implies that $|\theta_1| < 1$.

2.3 Model Building Strategy

In model building strategy of univariate time series, Box and Jenkins (1976,pp.17-18) suggested selecting a model which has smaller number of parameters, which they called a parsimonious model. They actually proposed an iterative procedure in model selection which includes the following stages.

- 1. Identification of the model
- 2. Estimation of the parameters
- 3. Diagnostic checking

2.3.1 Identification Problem

Box & Jenkins suggested identification of a preliminary model in this stage using ACF and PACF (partial autocorrelation function) pattern. The reason for using ACF and PACF are discussed below.

The MA(q) process can be defined as one of the form $u_{t} = \epsilon_{t} - \theta_{1} \epsilon_{t-1} - \theta_{2} \epsilon_{t-2} - \cdots - \theta_{\alpha} \epsilon_{t-\alpha}$

where, $\epsilon_{\rm t}$ are white noise (WN) with mean zero and constant variance σ^2 and also zero covariances.

Therefore,
$$E(u_t) = 0$$

$$Var(u_t) = E[u_t^2] = \sigma^2(1+\theta_1^2+\theta_2^2+\dots+\theta_q^2)$$

$$Cov(u_t u_{t-1}) = E[u_t u_{t-1}]$$

$$= E[(\epsilon_{t} - \theta_{1} \epsilon_{t-1} - \dots - \theta_{q} \epsilon_{t-q})(\epsilon_{t-1} - \theta_{1} \epsilon_{t-2} - \dots - \theta_{q} \epsilon_{t-q-1})$$

$$- \sigma^{2}[-\theta_{1} + \theta_{1} \theta_{2} + \dots + \theta_{q-1} \theta_{q}]$$

$$\bigcirc$$
 Cov($u_t u_{t-2}$) = E [$u_t u_{t-2}$]

$$= E[(\epsilon_{t}^{-\theta_{1}}\epsilon_{t-1}^{-} \cdots - \theta_{q}^{\epsilon_{t+q}})(\epsilon_{t-2}^{-\theta_{1}}\epsilon_{t-3}^{-} \cdots - \theta_{q}^{\epsilon_{t-q+2}})$$

$$= \sigma^{2}[-\theta_{2}^{+\theta_{1}}\theta_{3}^{+} \cdots + \theta_{q-2}^{-\theta_{q}}\theta_{q}^{-1}]$$

and so on.

Therefore, the autocorrelation function can be written as,

$$\rho_{k} = \frac{-\theta_{k} + \theta_{1} \theta_{k+1} + \dots + \theta_{q-k} \theta_{q}}{1 + \theta_{1}^{2} + \theta_{2}^{2} + \dots + \theta_{q}^{2}}, \quad k=1,2,\dots,q$$

$$= 0 , k > q$$

which implies that if the process is a moving average then we will have cuts-off in correlogram (plots of ACF) for the

autocorrelation with lag greater than q, the order of MA process.

 $= E[u_{t}(\phi_{1}u_{t-1}+\phi_{2}u_{t-2}+\dots+\phi_{p}u_{t-p}+\epsilon_{t}]$

 $= \phi_1 \gamma_1 + \phi_2 \gamma_2 + \dots + \phi_p \gamma_p + \sigma^2$

where, ϕ_1 , γ_2 ,, γ_p are the autocovariances with lag(1), lag(2),, lag(p) and ϕ_1 , ϕ_2 ,, ϕ_p are the autoregressive parameters.

 $\gamma_1 = \text{Cov}(u_{t-1}u_t)$ $= \mathbb{E}[(u_{t-1}(\phi_1u_{t-1} + \phi_2u_{t-2} + \dots + \phi_pu_{t-p} + \epsilon_t)]$ $= \phi_1 \gamma_0 + \phi_2 \gamma_1 + \dots + \phi_p \gamma_{p-1}$

 $\gamma_2 = Cov(u_{t-2}u_t)$

 $=\phi_1\gamma_1+\phi_2\gamma_0+\cdots+\phi_p\gamma_{p-2}$

 $\gamma_{p}^{=\phi_{1}}\gamma_{p-1}^{+\phi_{2}}\gamma_{p-2}^{+}\cdots + \phi_{p}^{}\gamma_{0}$

and for k > p

 $\gamma_k = \phi_1 \gamma_{k-1} + \phi_2 \gamma_{k-2} + \cdots + \phi_p \gamma_{k-p}$

Therefore, the autocorrelation functions for AR(p) process becomes (known as Yule-Walker equations),

$$\rho_{1} = \phi_{1} + \phi_{2} \rho_{1} + \dots + \phi_{p} \rho_{p-1}$$

$$\rho_{2} = \phi_{1} \rho_{1} + \phi_{2} + \dots + \phi_{p} \rho_{p-2}$$

$$\vdots$$

$$\rho_{p} = \phi_{1} \rho_{p-1} + \phi_{2} \rho_{p-2} + \dots + \phi_{p}$$
and for $k > p$

$$\rho_{k} = \phi_{1} \rho_{k-1} + \phi_{2} \rho_{k-2} + \cdots + \phi_{p} \rho_{k-p}$$

which implies that unlike MA process AR process does not have cuts-off in ACF for k > p. Therefore, we can conclude that if the ACF cuts off after a certain point the process can be thought of as an MA process. But, if it does not cut-off, rather dieing out slowly, it can be thought of as an AR process. More confirmation can be drawn from PACF.

Box and Jenkins suggested that the partial autocorrelation can be approximated by Yule-Walker estimates of the successive autoregressive process. This is discussed in detail by Pindyck and Rubinfield (1981,pp.524-526). For the pth order autoregressive process PACF has a cut-off after lag p. Box and Jenkins (1976,p.70) also show that for MA process PACF does not cut-off after lag q, rather dieing out slowly, as opposite to AR process.

Since we do not know the autocorrelation and partial autocorrelation in practice, we have to estimate them from the observation. But the estimated autocorrelation and partial autocorrelation will not necessarily be exactly zero. Rather, it will be approximately zero for k > q or p for MA process or AR process respectively.

Therefore we need to find the standard error of autocorrelation and partial autocorrelation estimates. Using Bartlett's approximation (see Box and Jenkins, 1976,pp.34-35) the variance of r_k (which is the estimated autocorrelation for ρ_k) is,

$$q$$

$$Var(r_k) \simeq [1+2 \sum_{i=1}^{\infty} \rho_i^2]/n, \qquad k > q.$$

For the autoregressive process we can use the result from Quenouille(see Box and Jenkins, 1976,p.65), that the variance of partial autocorrelation coefficient for lag period greater than the order p of the process can be approximated as, $\text{Var}[\hat{\phi}_{kk}] \simeq 1/n, \qquad k > p$

where n is the number of observations.

Recently, some other methods were proposed for identification of the model. One of them is Corner method proposed by Beguin, Gourierouse and Monfort (1980,pp.423-436) and another one is proposed by Pukkila (1982,pp.81-103). He

suggested that, since, specifically for mixed model it is difficult to get an idea about the order of the process using ACF and PACF, one should estimate the parsimonious models ARMA(p,q) beginning with one parameter model (either p=1, or q=1) and test whether the parameters are significantly different from zero and also test whether the estimated residuals behaves like white noise and if one of the above tests fails for all possible low order models, then proceed for higher order model. Thus, the models that could be checked are ARMA(0,1), ARMA(1,0), ARMA(1,1), ARMA(0,2) and so on. This seems to us to be reasonable, because, as Box-Jenkins and other authors agree, the models we have in practice have a small number of parameters. Since we have computer packages available to estimate the parameters quickly, we can use this technique too.

After tentatively identifying a model we can proceed to the next stage.

2.3.2 Estimation problem

Among the estimation methods frequently used for univariate time series analysis are the method of moments, the method of back forecasting, the method of least squares and the method of maximum likelihood(ML). The method of moments estimate for the first order moving average process is,

$$\hat{\theta} = \frac{-1 \pm \sqrt{1-4r_1^2}}{2r_1}$$

where, r₁ is the estimated autocorrelation coefficient of lag 1. From the above we see that there are two possible solutions, but only one of them will satisfy the invertibility condition. Box and Jenkins (1976,p.188) show that only one of the multiple moment solutions for any MA order will satisfy the invertibility condition. According to Judge, et. al. (1980,p.198) these estimates are inefficient relative to the Nonlinear Least Square (NLS) estimator. Most authors suggest using NLS or ML and to do this we need an initial estimate of the parameters.

Box-Jenkins suggest using the estimate obtained by the method of moments as an initial value of the parameters for NLS or ML.

We can obtain the preliminary estimates for AR process by solving the Yule-Walker equations discussed previously. Specifically, for AR(2) process these estimates are,

$$\hat{\phi}_1 = \frac{r_1(1-r_2)}{1-r_1^2}$$

$$\hat{\phi}_2 = \frac{r_2 - r_1^2}{1 - r_1^2}$$

In this paper, we will focus our attention upon the MA process.

A great deal of discussion has been given on nonlinear estimation technique in Box and Jenkins (1976,pp.231-242). Most of the computer packages use nonlinear least squares and not the maximum likelihood, because of the complexity in estimating the determinant of the covariance matrix for MA process.

4

Box and Jenkins (1976,p.213) suggested an approximation to the ML method by disregarding the determinant, because the determinant $|\Omega|$ is dominated by the exponent of the likelihood function. Mcleod(1977, pp.531-534) proposed a method by substituting an approximation of the determinant term in the likelihood function, claiming a closer approximation to the exact ML estimator. Osborn (1976,pp.75-87) uses the technique to calculate the exact covariance determinant mentioned by Box and Jenkins(1970,pp.270-272): $|\Omega| = |R'R|$, where, R is a matrix of order (n+q)xq, so that R'R is of order qxq and R can be calculated recursively. If n is big enough this technique might make problems in computer space and time in forming the R matrix recursively and also in multiplication of them. As a modification of this we will introduce a more efficient method to obtain the exact covariance determinant.

Another approach was given by Phadke and Kedem (1978,pp.511-519) for the moving average process. They get the transformation matrix by decomposing the covariance matrix Ω using the Cholesky decomposition and they also use the decomposed matrix to get the determinant. Later it was extended for ARMA model by Craig(1979,pp.59-65). Both of them use a library algorithm to decompose Ω .

In this paper later, we will show how the determinant can be easily obtained from the transformation procedure (used in Chapter 2 for GNL) without any further effort.

2.3.3 Diagnostic Checking

In this stage we test the model which we chose centatively, as to whether it appears to agree with the data.

The best way to investigate the adequacy of model fitting, is to observe its performance outside the sample period. That is, the whole sample is divided into two sets, one set is used for estimating the model and the other set is to check how well the model fits. But, most of the time insufficient amount of data prevents us from doing this. So, we use the same set of data for both the purposes.

Among the tests, we check whether the estimated parameters are significantly different from zero or not. Then we go for residuals checking, which should be WN, that is, to see that the residuals are as a whole uncorrelated among themselves. One of the test statistics suggested by Box and Pierce (1970) is, $Q_1(r) = n\sum\limits_{k=1}^m r_k^2$ where,

$$r_{k} = \frac{\sum_{t=1}^{\hat{\epsilon}} \hat{\epsilon}_{t} \hat{\epsilon}_{t-k}}{\sum_{t=1}^{n} \hat{\epsilon}_{t}^{2}}$$

and they showed that this statistic is asymptotically distributed as χ^2 with (m - p - q) d.f., where, p and q are the order of the AR and MA process respectively and m is the highest lag period for autocorrelation (i.e., the time displacement are 1,2,...,m) considered.

Later, Ljuny and Box (1978,pp.297-303) conclude that the test statistic,

$$Q_{2}(r) = n(n+2) \sum_{k=1}^{m} \frac{2}{n-k}$$

has better statistical properties than the above.

Pukkila (1982,pp.81-103) said that the above two statistics are not sensitive to slight departures from WN for reasonable sample size, thus, he proposed another test statistic under null hypothesis of WN,

$$Q_{3}(r) = \sum_{k=2}^{m} \frac{\left\{r_{k} - \hat{\phi}_{kk} + E(\hat{\phi}_{kk})\right\}^{2}}{Var(r_{k} - \hat{\phi}_{kk})}$$

where, ϕ_{kk} is the estimated partial autocorrelation at lag k and $m=2\sqrt{n}$, which he says reasonable for $50 \le n \le 100$. But, most computer packages use the Box-Pierce test for its simplicity.

Box and Jenkins also suggested overfitting the model, i.e., after identifying a model one has to select some other model around the identified one. If two models are identified to be selected then choose the one which has the smaller number of parameters.

2.4 Regression Equation with Moving Average Errors:

It can be observed that, recently, considerable attention has been given to the regression model with ARMA errors. Though the error process can be any of the three processes mentioned before, most researchers in practice assume the process to be autoregressive and most of the time a conclusion is drawn using the Durbin-Watson(DW) statistic proposed by Durbin and Watson(1950,1951). It is to be mentioned that the DW-statistic is not valid for the error process other than AR(1); see Koutsoyiannis(1977,pp.212,216). Harvey (1981,p.209-210) also expressed the same view. Therefore the DW-statistic is sometimes misleading. In the case where the lag dependent variable appears as an independent variable, Durbin(1970) suggested another test-statistic. Wallis (1972) developed a test-statistic for the seasonal fourth order autocorrelation in the error term of a regression equation etimated from quarterly data, generalizing the DW-statistic. Since most computer packages provide a test and estimation technique for the AR(1) process, most researchers assume that the underlying process of regression error is AR(1), as mentioned by Harvey(1981,p.189), though there is no reason why the other processes should not be entertained equally. Under these circumstances, researchers became interested in exploring the other areas and some related works are Phillips (1966), Aigner(1971), Pagan(1973), Pierce(1971), Pagan(1974), Nicholls, Pagan and Terrel (1975) and Pagan & Nicholls (1976).

The model we considered for this paper is the regression model with MA errors. Until recently, little work have been done on higher order MA process. Almost all the Monte Carlo or similar kinds of numerical comparisons were done on the MA(1) process. We will attempt a Monte Carlo comparison for three different procedures discussed below for the MA(2) process.

Most of the time transformations developed for MA(1) are difficult, sometimes impossible to generalize for higher order; e.g., Balestra(1980), Pesaran(1973), which is also mentioned by Judge(1980,p.196). But the transformation we are proposing in this paper does not need the inversion of a matrix nor even the transformation matrix and can easily be implemented for higher order MA process.

2.4.1 Regression Model

Let us consider a regression model,

$$Y = X\beta + U$$

(2.3)

Where, Y is a response vector of dimension nx1

X is a nonstochastic design matrix of dimension $n \times k$ with rank k, k < n

U is a random vector of dimension nx1

 β is a parameter vector of dimension kx1

i.e.,

$$Y = \begin{bmatrix} Y_1 \\ Y_2 \\ Y_3 \\ Y_4 \\ Y_5 \\ \vdots \\ Y_n \end{bmatrix} \qquad \begin{array}{c} u = \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \\ u_5 \\ \vdots \\ u_n \\ \end{array} \qquad \begin{array}{c} \beta = \begin{bmatrix} \beta_1 \\ \beta_2 \\ \beta_3 \\ \beta_4 \\ \vdots \\ \beta_k \\ \end{array}$$

and assume the disturbance term U follows a second order moving average process,

$$u_{t} = \epsilon_{t} - \theta_{1} \epsilon_{t-1} - \theta_{2} \epsilon_{t-2}$$
 (2.4)

The random variable ϵ_{t} is assumed to be independent with zero mean and constant variance, i.e., $E(\epsilon_{t}) = 0$, $Var(\epsilon_{t}) = \sigma^{2}$. Therefore, the random vector u_{t} is thus characterized by,

 $E(u_{+}) = 0$ and $E(u_{+} u_{+}') = \sigma^{2} \Omega$.

 Ω is a five-diagonal matrix, with $1+\theta_1^2+\theta_2^2$ in the main diagonal, $-\theta_1(1-\theta_2)$ in the second diagonal above and below the main diagonal and $-\theta_2$ in the third diagonal above and below the second diagonal. This follows since,

$$E(u_t u_t) = E(u_t^2) = (1 + \theta_1^2 + \theta_2^2) \sigma^2$$

$$\mathbb{E}\left(\mathbf{u}_{\mathsf{t}} \quad \mathbf{u}_{\mathsf{t-1}}\right) = \mathbb{E}\left[\left(\boldsymbol{\epsilon}_{\mathsf{t}}^{-\boldsymbol{\theta}}, \boldsymbol{\epsilon}_{\mathsf{t-1}}^{-\boldsymbol{\theta}}, \boldsymbol{\epsilon}_{\mathsf{t-2}}^{-\boldsymbol{\theta}}, \boldsymbol{\epsilon}_{\mathsf{t-2}}^{-\boldsymbol{\theta}}, \boldsymbol{\epsilon}_{\mathsf{t-2}}^{-\boldsymbol{\theta}}, \boldsymbol{\epsilon}_{\mathsf{t-3}}^{-\boldsymbol{\theta}}, \boldsymbol{\epsilon}_{\mathsf{t-3}}^{-\boldsymbol{\theta}},$$

$$= -\theta_1 E(\epsilon_{t-1})^2 + \theta_1 \theta_2 E(\epsilon_{t-2})^2 + 0 + 0 + \dots$$

$$= -\theta_1 \sigma^2 + \theta_1 \theta_2 \sigma^2$$
, (since ϵ_t is homoscedastic),

$$= -\theta_1 (1-\theta_2) \sigma^2$$

$$E(u_t u_{t-2}) = -\theta_2 \sigma^2$$

$$E(u_t u_{t-3}) = 0$$

 $E(u_t u_{t-n}) = 0$

2.5 Different Procedures for Transformation

It is well known that an analytical expression for the transformation to transform the generalized regression problem into a simple(OLS) regression problem is generally available for the regression model with autoregressive disturbances. See J. Wise (1955)² for Ω^{-1} and Fuller (1976,p.423) for this transformation. However, an analytical expression for such a transformation in the case of a regression model with moving average disturbances is available only for the first order, i.e., for MA(1) disturbances Balestra (1980). Pesaran (1973) also found the transformation matrix for the first order moving average process, and that involves more complexity than Balestra's method. Both the above procedures have a limitation in the sense that they are not readily extended for higher order MA process.

¹By different procedures we mean the different ways of transformation of a generalized regression problem into a simple regression problem; in other words, the procedure is a way of writing down the model equations (2.3) and (2.4) so that the resulting model becomes an OLS problem.

²This inverse matrix is also given in Kendall, Stuart and Ord(1983.p.543)

The estimation of regression coefficients when the regression model has moving average process disturbances can be handled in several ways. We will discuss the following three procedures:

- a) General Procedure
- b) MacDonald and MacKinhon Procedure
- c) Phillips Procedure

2.5.1 General Procedure

To retain the BLUE (Best Linear Unbiased Estimate) properties of regression coefficient with white noise error, we need to transform the original observations so that the regression residuals after transformation becomes white noise (W.N.).

Let T be a non-singular matrix such that,

$$T\Omega T' = I_{D}$$

or.
$$T^{-1}T\Omega T' = T^{-1}$$

or,
$$I\Omega T'(T')^{-1} = T^{-1}(T')^{-1}$$

or,
$$I\Omega I = T^{-1}(T')^{-1}$$

or,
$$\Omega = (T'T)^{-1}$$

or,
$$\Omega^{-1} = T'T$$

The transformed model is then,

$$TY = TX\beta + TU$$

and the covariance matrix of transformed residual is,

$$E[TU(TU)'] = E[TUU'T']$$

$$=T E(UU') T'$$

$$=T \sigma^{2}\Omega T'$$

$$=\sigma^{2} T\Omega T'$$

$$=\sigma^{2} I_{n}$$

The Ordinary Least Square (OLS) estimate of regression co-efficient on transformed observation is,

$$\beta = [(TX)'(TX)]^{-1} (TX)'TY$$

$$= [X'T'TX]^{-1} X'\Omega^{-1}Y$$

$$= [X'\Omega^{-1}X]^{-1} X'\Omega^{-1}Y$$

called GLS estimate (see Goldberger, 1963, p.232-234).

2.5.1.1 Transformation Matrix

To get the transformation matrix we can proceed as follows:

There exists a uniquely defined positive upper triangular

matrix S (i.e., upper triangular with positive diagonal elements)

such that,
$$S'S = \Omega$$

or, $S = (S')^{-1} \Omega$

Since, Ω is a (2q+1)-diagonal symmetric band matrix, S is an upper triangular matrix with non-zero elements in the main diagonal and also the q diagonals immediately above the main diagonal are non-zero and all other elements are zero; S' is a similar kind of lower triangular matrix and therefore, $(S')^{-1}$ is also a lower triangular matrix.

From the relationship,

$$S = (S')^{-1} \Omega$$

assuming we have S and Ω , we can solve recursively for the elements of the matrix $(S')^{-1}$, which is our required transformation matrix.

Again we know that, $S S^{-1} = I$, therefore, solving for the elements of S^{-1} from the equation system we could get the transformation matrix, which would be more efficient than the above computation. However, we did not use either of these two transformation matrices in the simulation experiment, because the recursive transformation (described below) is simpler and easier to implement.

2.5.1.2 Transformation in Recursive Form

The transformation in a recursive way is so simple that it avoids the inversion of Ω and even the transformation matrix. Then all we need to obtain $\sqrt{\Omega}$ which we denote as S, are the

values S_{ij}. For practical purposes the transformation can be shown in simple recursive way as below;

$$Y_1 = Y_1/s_{11}$$

$$Y_2 = (Y_2 - s_{12} Y_1)/s_{22}$$

$$Y_3 = (Y_3 - s_{23} Y_2 - s_{13} Y_1)/s_{33}$$

$$Y_4 = (Y_4 - s_{34} Y_3 - s_{24} Y_2 - s_{14} Y_1)/s_{44}$$

$$Y_5 = (Y_5 - s_{45} Y_4 - s_{35} Y_3 - s_{25} Y_2-s_{15} Y_1)/s_{55}$$

where, Y and Y are the transformed and original observations respectively; q is the order of MA process and n is the number of observations. Similarly, we can get the transformed variable for each column of the X-matrix.

The square root matrix S of Ω could easily be obtained from the relationship ,

$$\Omega = S'S$$
.
Since, $\Omega_{ii} = S_{1i}^{2} + S_{2i}^{2} + S_{3i}^{2} + \dots + S_{ii}^{2}$, $i = j$

and
$$\Omega_{ij} = S_{1i} S_{1j} + S_{2i} S_{2j} + S_{3i} S_{3j} + \dots + S_{ii} S_{ij}$$
, i

we have,

$$S_{11} = \sqrt{\Omega_{11}}$$
 and $S_{1j} = \Omega_{1j} / S_{11}$, $i=1$

$$S_{1i} = \sqrt{(\Omega_{ii} - \sum_{k=1}^{i-1} S_{ki}^2)}$$
, $i > 1$

$$S_{ij} = (\Omega_{ij} - \Sigma S_{ki} S_{kj})/S_{ii} , i > 1 \text{ and } j > i$$

$$k=1$$

 S_{ij} = 0, i > j and j > i+q, where q is the order of MA process. Specifically, for MA(2) the S_{ij} 's are, $S_{11} = \sqrt{\Omega_{11}}$, i=1

$$S_{22} = \sqrt{(\Omega_{11} - S_{12}^2)}$$
, $i=2$

$$S_{i,i} = \sqrt{(\Omega_{11} - S_{i-2,i}^2 - S_{i-1,i}^2)}$$
, $i = 3,4,5,...,n$

$$S_{12} = \Omega_{12}/S_{11}$$
 , i = 2

$$S_{i-1,i} = (\Omega_{12} - S_{i-2,i-1} S_{i-2,i}) / S_{i-1,i-1}$$
, $i = 3,4,5,...,n$

$$S_{i-2,i} = \Omega_{13}/S_{i-2,i-2}$$
, $i = 3,4,5,...,n$

In particular, for second order moving average process the recursive transformation can be shown as follows:

$$Y_1 = Y_1/S_{11}$$

$$Y_2 = (Y_2 - S_{12}Y_1)/S_{22}$$

$$Y_{i} = (Y_{i} - S_{i-1}, i Y_{i-1} - S_{i-2}, i Y_{i-2}) / S_{ii}$$
, $i = 3, 4, 5, \dots, n$.

One can use a library subroutine to calculate the elements of S_{ij} (square root matrix of Ω) to get the transformation. But as we observe from the above algebra, a self contained program can be written to get the transformation without using library subroutine and the computer program is given in Appendix H.1 for transformation in the case of MA(2) process. The above model equations may then be analysed as described in Section 2.6.1.

2.5.2 MacDonald & MacKinnon Procedure

MacDonald and MacKinnon(1985) propose a very simple procedure to deal with MA(1) residuals in regression equation by GLS.

Without using the matrix M for transformation in Osborn's paper (1978) for univariate time series model, which is tedious to form and also needs computer space, one can use the recursive form of transformation, as MacDonald and MacKinnon did in their paper for MA(1) and we will extend MacDonald and Mackinnon procedure for higher order MA process.

The model to be considered here is same as previous one,

$$Y_{t} = X_{t}\beta + U_{t}$$
 (2.5)

where,
$$U_t = \epsilon_t - \theta_1 \epsilon_{t-1} - \theta_2 \epsilon_{t-2} - \cdots - \theta_q \epsilon_{t-q}$$
 (2.6)

We can combine the above two equations into $\Upsilon = X\beta + Z'\eta + \epsilon$; with some algebra one can verify that this represents (2.5) and '(2.6) when the transformed variables Υ , X and Z are defined and calculated recursively as follows:

$$\Upsilon_t = \Upsilon_t + \theta_1 \Upsilon_{t-1} + \theta_2 \Upsilon_{t-2} + \dots + \theta_q \Upsilon_{t-q}$$

$$X_t = X_t + \theta_1 X_{t-1} + \theta_2 X_{t+2} + \dots + \theta_g X_{t-q}$$

$$Z_t = \Theta Z_{t-1}$$
, where,

$$\Theta = \begin{bmatrix} \theta_1 & 1 & 0 & 0 & \dots & 0 \\ \theta_2 & 0 & 1 & 0 & \dots & 0 \\ \theta_3 & 0 & 0 & 1 & \dots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\ \theta_{q-1} & 0 & 0 & 0 & \dots & 1 \\ \theta_q & 0 & 0 & 0 & \dots & 0 \end{bmatrix}$$

gxg

$$= \begin{bmatrix} \theta_{q-1} & I \\ \theta_q & 0 \end{bmatrix}$$

where, θ_{q-1} is a column vector of θ_1 , θ_2 θ_3 θ_{q-1} , I is a identity matrix of order (q-1)x(q-1), θq is a scalar and '0' is a row vector of zeroes of (q-1) elements;

$$\mathbf{Z}_{0} = \begin{bmatrix} -1 \\ 0 \\ 0 \\ 0 \\ \vdots \\ \vdots \\ 0 \end{bmatrix} \quad \eta = \begin{bmatrix} \epsilon_{0} \\ \epsilon_{-1} \\ \vdots \\ \epsilon_{-2} \\ \vdots \\ \epsilon_{-q+1} \end{bmatrix}$$

 \mathbf{Y}_0 , \mathbf{Y}_{-1} ,, \mathbf{Y}_{-q+1} and \mathbf{X}_0 , \mathbf{X}_{-1} ,, \mathbf{X}_{-q+1} being zeroes.

In particular for MA(2) process the above procedure can be described as below,

The model is,

$$Y_t = X_t \beta + U_t$$

 $U_t = \epsilon_t - \theta_1 \epsilon_{t-1} - \theta_2 \epsilon_{t-2}$ and the combination of the above two equations is,

where,

$$Y_t = Y_t + \theta_1 Y_{t-1} + \theta_2 Y_{t-2}$$

$$X_t = X_t + \theta_1 X_{t-1} + \theta_2 X_{t-2}$$

$$\mathfrak{T}_{+} = \Theta \mathfrak{T}_{+-1}$$

$$\Upsilon_0 = \Upsilon_{-1} = 0$$

$$X_0 = X_{-1} = 0$$

$$\mathcal{Z}_{0} = \begin{bmatrix} -1 \\ 0 \end{bmatrix} \qquad \eta = \begin{bmatrix} \epsilon_{0} \\ \epsilon_{-1} \end{bmatrix} \qquad \Theta = \begin{bmatrix} \theta_{1} & 1 \\ \theta_{2} & 0 \end{bmatrix}$$

These model equations may then be analysed as described in Section 2.6.2.

2.5.3 Phillips Procedure

This procedure was first introduced by Phillips(1966) and applied by Trivedi(1970), further studied by Pagan & Nicholls (1976).

, in

The regression error u_t , which follows MA process, $u_t = \epsilon_t - \theta_1 \epsilon_{t-1} - \theta_2 \epsilon_{t-2} - \cdots - \theta_q \epsilon_{t-q}$

can be written as,

$$U = M \epsilon - \widetilde{M} \widetilde{\epsilon}$$

where, $U' = [u_1 \ u_2 \ u_3 \ \dots \ u_n]$ $\epsilon' = [\epsilon_1 \ \epsilon_2 \ \epsilon_3 \ \dots \ \epsilon_n]$

$$\tilde{\epsilon}' = [\epsilon_0 \quad \epsilon_{-1} \quad \epsilon_{-2} \quad \dots \quad \epsilon_{-q+1}]$$

Pagan and Nicholls establish a theorem, that minimizing $\epsilon'\epsilon+\widetilde{\epsilon}'\widetilde{\epsilon}$ with respect to β , θ and $\widetilde{\epsilon}$ is equivalent to minimizing $U'\Omega^{-1}U$ with respect to β and θ , therefore NLS or ML can be applied by calculating the errors in the sum of squares $\epsilon'\epsilon+\widetilde{\epsilon}'\widetilde{\epsilon}$ recursively as follows:

$$\begin{aligned}
\epsilon - q + 1 &= \widetilde{\epsilon} - q + 1 \\
\cdot \cdot \cdot \cdot \\
\epsilon - 1 &= \widetilde{\epsilon} - 1 \\
\epsilon_0 &= \widetilde{\epsilon}_0
\end{aligned}$$

$$\begin{aligned}
\epsilon_1 &= y_1 - x_1' \beta + \sum_{j=1}^{\infty} \theta_j \widetilde{\epsilon}_{1-j} \\
\vdots &= 1
\end{aligned}$$

$$\epsilon_{t} = y_{t}^{-x} x_{t}^{'\beta} + \sum_{j=1}^{T} \theta_{j} \epsilon_{t-j} + \sum_{j=1}^{T} \theta_{j} \epsilon_{t-j}^{\epsilon}, t=2,3, \dots, q$$

$$\epsilon_{t} = y_{t} - x_{t}' \beta + \sum_{j=1}^{q} \epsilon_{t-j}, t = q+1, q+2, \dots, n$$

$$j=1$$

To calculate the above residuals one needs to have starting values for the vector $\tilde{\epsilon}$. One possibility is to set $\tilde{\epsilon}=0$ and the other way is to estimate $\tilde{\epsilon}$. To estimate $\tilde{\epsilon}$ we can use back forecasting method discussed by Box & Jenkins (1970,p.213-215), which will be more efficient than setting $\tilde{\epsilon}=0$. Osborn's (1978) method using least squares can also be used to estimate $\tilde{\epsilon}$.

In particular for MA(2)—process, the successive residuals are defined by,

$$\epsilon_{-1} = \epsilon_{-1}$$

$$\epsilon_{0} = \epsilon_{0}$$

$$\epsilon_{1} = y_{1} - \beta_{0} - x_{1} \beta + \theta_{1} \epsilon_{0} + \theta_{2} \epsilon_{-1}$$

$$\epsilon_{2} = y_{2} - \beta_{0} - x_{2} \beta + \theta_{1} \epsilon_{1} + \theta_{2} \epsilon_{0}$$

$$\epsilon_{3} = y_{3} - \beta_{0} - x_{3} \beta + \theta_{1} \epsilon_{2} + \theta_{2} \epsilon_{1}$$

$$\epsilon_{n} = y_{n} - \beta_{0} - x_{n} \beta + \theta_{1} \epsilon_{n-1} + \theta_{2} \epsilon_{n-2}$$

These model equations may then be analysed as described in Section 2.6.3.

2.6 Method of Estimation

As a method of estimation we considered Estimated

Generalized Least Squares (EGLS) and Maximum Likelihood (ML).

Details of these two methods for three different Procedures is given below.

2.6.1 General Procedure

2.6.1.1 Estimated Generalized Least Square(EGLS):

Here, we transform the original observations replacing θ by its estimate, $\hat{\theta}$. One possible estimator of θ is,

$$\hat{\theta} = \frac{1 - \sqrt{(1 - 4\hat{\rho}_1^2)}}{2\hat{\rho}_1}$$

where, $\hat{\rho}_1$ is the autocorrelation coefficient of OLS errors for one period lag. This estimator is used by MacDonald and MacKinnon, Judge and others for MA(1). For MA(2) a similar kind of estimate can be obtained by solving the nonlinear equations,

$$\rho_1 = \frac{-\theta_1(1-\theta_2)}{1+\theta_1^2+\theta_2^2}$$

$$\rho_2 = \frac{-\theta_2}{1 + \theta_1^2 + \theta_2^2}$$

for θ_1 and θ_2 , but the estimated values for θ_1 and θ_2 can be read off directly from 'Chart C' at the end of the book by Box and Jenkins (1970,p.519). According to Judge(1980,p.198) these estimates are inefficient relative to the NLS estimator and also it is very difficult to get the estimates for θ 's as the order of the moving average process increases. Therefore, it could be suggested that, since there are many computer packages (e.g., MINITAB) which can easily give us the NLS estimate of θ 's we can use these packages to get the estimates of θ 's to use in the transformation.

Therefore, the EGLS estimate of regression coefficient is $\beta = (X'X)^{-1}X'Y \text{ where, } X = TX, Y = TY \text{ and } T \text{ is the estimated}$ transformation matrix $T = T(\theta)$.

2.6.1.2 Maximum Likelihood:

Under the assumption of normality, log-likelihood function deleting the constant can be written as,

$$L(\beta,\Theta,\sigma^2) = -\frac{n}{2} \ln \sigma^2 - \frac{1}{2} \ln |V| - \left[\frac{1}{2\sigma^2} (\Upsilon - X\beta)' (\Upsilon - X\beta)\right].$$

Where V is defined as before the estimated covariance matrix Ω . Now replacing σ^2 by its ML estimator,

$$\hat{\sigma}^2 = \frac{(Y - X\beta)'(Y - X\beta)}{2},$$

after some simplifications the log-likelihood function becomes, $L(\beta,\Theta) = -\frac{n}{2} \ln[|V|^{(1/n)}(\Upsilon - X\beta)'(\Upsilon - X\beta)].$

Therefore maximizing the above likelihood is equivalent to minimizing $|V|^{(1/n)}(\Upsilon-X\beta)'(\Upsilon-X\beta)$ with respect to β and Θ . A computer program e.g., FORTRAN subroutine from NAG, for mimimizing the above objective function, can give us the ML estimate of β and Θ , where β and Θ are the vectors of regression and MA parameters respectively.

2.6.2 MacDonald & MacKinnon Procedure

2.6.2.1 Estimated Generalized Least Square (EGLS):

We will use the same estimator of θ 's as we did in the General Procedure, and using the transformation technique discussed in Section 2.5.2 we have the transformed model, $\Upsilon = X\beta + \Upsilon' \eta + \epsilon.$

Now by applying Ordinary Least Squares on transformed variables we can obtain the estimates of β and η .

2.6.2.2 Maximum Likelihood:

Under the assumption of normality, log-likelihood function after deleting constant term can be written as,

$$L(\beta,\Theta,\eta) = -\frac{n}{2} \ln[|V|^{(1/n)}(Y-X\beta-Z'\eta)'(Y-X\beta-Z'\eta)]$$

where β , Θ and η are vectors of parameters.

Therefore, maximizing the above log-likelihood is equivalent to minimizing $|V|^{(1/n)}(Y-X\beta-Z'\eta)'(Y-X\beta-Z'\eta)$ with respect to β , θ and η .

2.6.3 Phillips Procedure

2.6.3.1 Estimated Generalized Least Square(EGLS) (or NLS):

Since the sum of squares of errors becomes $\epsilon'\epsilon+\widetilde{\epsilon}'\widetilde{\epsilon}$ and we can calculate them recursively as shown in Section 2.5.3, we can minimize the above sum of squares with respect to β , θ and $\widetilde{\epsilon}$ using a minimization program to obtain the EGLS (or NLS) estimates of the parameters.

2.6.3.2 Maximum Likelihood:

Under the assumption that ϵ_{t} are normally distributed, the log-likelihood function can be written as,

$$L(\beta,\Theta,\widetilde{\epsilon}) = -\frac{n}{2} \ln(2\pi\sigma^2) - \frac{1}{2} \ln|V| - \frac{\epsilon'\epsilon + \widetilde{\epsilon}'\widetilde{\epsilon}}{2\sigma^2}$$

Now, replacing σ^2 by its ML estimator

$$\hat{\sigma}^2 = \frac{\epsilon' \epsilon + \tilde{\epsilon}' \tilde{\epsilon}}{n},$$

the log-likelihood function can be written as $L(\beta,\Theta,\widetilde{\epsilon}) = -\frac{n}{2} \ln[|V|^{(1/n)}(\epsilon'\epsilon+\widetilde{\epsilon}'\widetilde{\epsilon})].$

Therefore, maximizing the above log-likelihood is equivalent to minimizing $|V|^{(1/n)}(\epsilon'\epsilon+\tilde{\epsilon}'\tilde{\epsilon})$ with respect to β , Θ and $\tilde{\epsilon}$.

2.7 SIMULATION EXPERIMENT:

The simulation experiment is carried out for small samples as well as for moderate samples, with MA(2) error process in a regression model, to compare the performance of three different procedures. For small sample we choose size 10, and 50 as a moderate size.

In this experiment for simplicity the regression model considered is,

$$Y_t = \beta_0 + \beta_1 X_t + U_t$$
; where, $U_t = \epsilon_t - \theta_1 \epsilon_{t-1} - \theta_2 \epsilon_{t-2}$

In the above model we specified the value of the regression parameters β_0 = 0 and β_1 = 5.

For each of the sample sizes both the moving average parameters, namely θ_1 and θ_2 are made to vary as below;

we choose θ_2 as -0.50 and -0.80. For each θ_2 , θ_1 takes values ± 1.45 and ± 1.15 . Therefore we have eight different pairs of θ 's and for each pair of θ 's we generate 100 samples (repetitions) of same size.

The different stages involved in this experiment are discussed below:

a) Stage-I:

This stage involves computing of u_t from ϵ_t a random variable with mean zero and unit variance from a normal population using a specified pair of θ 's. ϵ_t is obtained by using the MINITAB computer package. Then using the specified values of regression parameters and a set of X_t adding with u_t

we can obtain the response vector Y_t for each pair of θ 's. Thus we are introducing MA(2) error in our regression model.

b) Stage-II:

In this stage we regress Y on X (OLS) to estimate the regression error $\hat{\mathbf{u}}$, which will be used to identify and estimate MA parameters. To identify the order of the process we use the identification criteria discussed in Chapter-2 and estimate the θ 's from regression errors using BMDQ2T computer package.

c) Stage- III:

Now, we apply three procedures, which were discussed in Section 2.5 and obtain the estimated values of the regression coefficients for each pair of θ 's and for two different sample sizes mentioned above.

2.8 Empirical Results:

Here, we have reported the results found by the simulation experiment. We will discuss the performance of different procedures through efficiency in two ways, efficiency due to variance of regression coefficient and efficiency due to computational time (i.e., cpu time).

From Appendix A.1 to Appendix A.8, it can be inferred that the regression coefficients are virtually unbiased regardless of the procedure and of the θ values considered. But it can be noticed that as the sample size increases the amount of bias decreases though the amount of bias is very small even for

sample size 10.

Concerning efficiency (due to variance), we use the relative efficiency of regression coefficients of a particular procedure with respect to the OLS (i.e., estimated variance of regression coefficient obtained by OLS divided by the estimated variance of regression coefficient obtained by using a particular procedure from 100 repetitions).

For the sample size 50, all three procedures are more or less the same in efficiency gain, though GNL (General) performs better in most of the cases and all three procedures perform better than OLS.

When sample size is 10 (Appendix A.1 to Appendix A.4), the efficiency gain by GNL (General) is higher over MM (MacDonald and MacKinnon) for both EGLS and ML and for all the pairs of θ 's considered, but, GNL(ML) is slightly less efficient than PHL(ML) (Phillips) in two cases, equal in two cases and better in four cases, though the difference is very small. It is also observed that PHL(ML) gives regression estimates identical with GNL(ML) in more than 95% of the samples. It is hard to justify the comparison of PHL(NLS) with EGLS of other two, because PHL(NLS) has several iterations, whereas GNL and MM need only two OLS regression for EGLS. But it can be noticed that PHL(NLS) does better than GNL(EGLS) and MM(EGLS) when θ_1 takes positive value and does poorly than GNL(EGLS) when θ_1 takes negative value. For the same sample size (n=10) efficiency gain is higher by ML than by EGLS for both the procedures (GNL and MM) except the cases

(at Appendix A.2) $\theta_{\chi} = -1.15$, $\theta_{2} = -.50$ and (at Appendix A.4) when $\theta_{1} = -1.15$ and $\theta_{2} = -.80$, where OLS performs better than MM; the reason may be that most of the time θ_{2} lies on the boundary of the invertibility region. In this context it can be mentioned that MacDonald and MacKinnon in their paper (1985, for MA-1) also found that OLS performs better than EGLS when θ is negative and MM(EGLS) performs very badly when $\theta = -.80$ and n = 100.

Another interesting behaviour is that, when sign of θ 's are different i.e., when θ_1 is positive and θ_2 negative (we consider only negative θ_2 in this paper), the efficiency gain with intercept and slope are same, though the tendency is higher for intercept. But, when the sign of θ_1 is negative, efficiency with slope is always higher than with intercept and the difference is much more as the sample size increases.

Since the results obtained form a complicated structure we also use covariance analysis to summarize our results. In this summarization we shall use terms like "significance" rather loosely, This is not a pretense of probability sampling or of genuine inference, but only a means of summarizing the extent to which the pattern emerging from our simulations conforms to the additive ANOCOVA model described. The dependent variables considered for the model below are:

a) Relative efficiency for intercept, b) Relative efficiency for slope, c) Bias for intercept and d) Bias for slope (absolute bias is used). The independent variables are sample size, value of θ_2 , sign of θ_1 , magnitude of θ_1 and six different methods as

a categorical variable, namely, GNL(EGLS), GNL(ML), MM(EGLS), MM(ML), PHL(NLS) and PHL(ML). In more detail, in Appendices B.1 and B.2 the additive model,

Y = constant + T; + (SMS2 x coefficient) + (TH2 x coefficient) + (STH1 x coefficient) + (MTH1 x coefficient) + error was imposed upon our simulated results, as a mechanical device for organizing and presenting our results. Here, Σ T; = 0, so that T; is the "effect" of using method number as below,

 $\overline{T_1} = GNL(EGLS)$

 $T_2 = GNL(ML)$

 $T_3 = MM(EGLS)$

 $T_{\Lambda} = MM(ML)$

 $T_5 = PHL(NLS)$

 $T_6 = PHL(ML)$

and also,

SMSZ = sample size

TH2 = specific value of θ_2

 $_{r}$ STH1 = sign of θ_{1}

MTH1 = magnitude of θ_1

In Appendices B.3 to B.6 similar but separate analyses were performed, first for all the simulated samples of size 10 and then for all the simulated samples of size 50.

When bias is concerned from the ANOCOVA table (Appendix B.2), we see that, for all the six methods the value of the estimated effects of method on bias are so small that they can be ignored. The significance levels suggest that the

coefficients are not significantly different from zero for both intercept and slope. But for sample size (SMSZ, which is an independent variable), significance levels indicate that sample size has significant effect on bias, though it is very very small. The sign of the coefficient is negative, indicating the inverse relationship with the dependent variable, so that as the sample size increases bias decreases, which supports our previous discussions, which were based on informal examination without using ANOCOVA. Aga n the significance level for sign of θ_1 (for intercept) tells us that the sign of θ_1 has influence on the amount of bias. But, since all the estimated coefficients for bias as dependent variable are so small we can ignore their effects.

In the case of efficiency gain for both intercept and slope by different procedures, it can be observe that (Appendix B.3) the estimated coefficient .25640 for GNL(ML) and .25265 for PHL(ML) (for intercept), and (for slope) the estimated coefficient .56810 for GNL(ML) and .49023 for PHL(ML) with significant t-statistic puts the GNL(ML) in the top rank for the sample size 10. This can again be verified by examining Appendix A.1 to Appendix A.4, where for four pairs of θ 's GNL(ML) does better than PHL(ML), for two pairs of θ 's they are same and for two pairs of θ 's GNL(ML) could not perform better than PHL(ML), though the amount of relative efficiency is almost the same. Therefore, considering all the eight pairs of θ 's GNL(ML) is marginally superior than PHL(ML).

For the same sample size, both GNL(ML) and PHL(ML) performs better than MM(ML) for all pairs of θ 's. Again considering EGLS, GNL performs better than MM for both the sample sizes and for all pairs of θ 's considered (Appendices A.1 to A.8).

The significance levels (Appendix B.1) for sample size (SMSZ) in both intercept and slope indicates the certainty of sample size's effect on efficiency gain, though the estimated values of the coefficients are very small, but the positive sign indicates that as sample size increases efficiency gain also increases. The magnitude of θ_1 (MTH1) also has a significance level which shows strong suggestion of positive effect upon efficiency gain and the value of the estimated coefficient is as high as 23.982 (Appendix B.1) for slope efficiency (also high for intercept efficiency) with positive sign. This indicates that for high values of θ_1 efficiency gain is higher for both slope and intercept, which is very effective when sample size gets large (see Appendix B.3 and Appendix B.5).

Sign of θ_1 (STH1) also has a definite effect for intercept efficiency gain (looking through significance level) and the value of the coefficient is 2.657 (Appendix B.1) with positive sign. This suggests that, as long as the sign for θ_1 is positive, efficiency gain is higher than for negative and this is true for both the sample sizes (Appendix B.3 and Appendix B.5) and for sample size 50 the estimated coefficient is as high as 4.905. It can be further confirmed by looking through the Rel. Efficiency table (Appendix A.1 to Appendix A.4), for sample

size 10 (except for one case θ_2 =-.50, θ_1 = ±1.45 in GNL(ML)) that efficiency gain with intercept is higher when θ_1 is positive. This can also be seen when n=50 (Appendix A.5 to Appendix A.8). It is observed that for all pairs of θ 's and for each method, efficiency gain with intercept is higher for positive θ_1 and the difference is more as the magnitude of θ_1 goes up. This is also true for slope efficiency i.e., as the magnitude of θ_1 increases the amount of relative efficiency increases (Appendix A.5 to Appendix A.8, n=50) in every case and for all methods. This is further confirmed by the ANOCOVA table (Appendix B.5, n=50), where with very much favourable significance level and an estimated coefficient of 47.128 the positive sign tells us that as θ , increases in magnitude efficiency gain also increases. But with slope efficiency for sign of θ_1 (Appendix B.1), significance level is not favourable and the estimated value of the coefficient has a negative sign. Therefore with a non-significant significance level and a small estimated coefficient (as -.765), it appears that the sign of θ , virtually has no effect on efficiency gain with slope.

For the value of θ_2 (TH2), which appears as an independent variable in the model described above, the significance level (Appendix B.1, for the combined samples) confirms the effect on slope efficiency but not on intercept efficiency, though the estimated value of the coefficients is high for both with positive sign. Again, for sample size 10 (Appendix B.3) the estimated coefficients of the TH2 variable are very small and

the signs are negative, whereas for sample size 50 (Appendix B.5) the estimated coefficients are high with positive sign, for slope it is as high as 23.146 and is confirmed through significance level. Therefore, it is tempting to draw the conclusion with sample size 50, that as θ_2 increases (decreases in magnitude) the efficiency gain is higher, but if we look to the results in Appendix A.5 to Appendix A.8, specifically for slope, when θ_1 = ±1.15, then as θ_2 goes from -.50 to -.80 efficiency increases (Appendix A.6 and Appendix A.8) and for θ_1 = ±1.45 ef-iciency decreases for the same change of θ_2 (Appendix A.5 and Appendix A.7). Therefore, it is difficult to draw any conclusion only with two values of θ_2 and at the same time ignoring θ_1 .

If we consider computing efficiency, i.e., the cpu time required for the computations, using the method EGLS for GNL and MM procedure, it seems that both procedures are more or less the same in cpu time requirement and they need a fraction of a second. Since ML or NLS needs several iterations and therefore more cpu time, we recorded the cpu time (in IBM-3081) for different procedures in Appendix A.1 to Appendix A.8. For sample size 10 GNL(ML) takes always less time than the others and in general all methods take less time when θ_1 is negative. If we consider rank of taking less cpu time, it is GNL(ML), PHL(ML) and MM(ML) respectively for both sample sizes. It is also observed that as sample size increases the time requirement is also increased, but the proportion of time requirement more or

less remains same among the three procedures.

Now, if we bring PHL(NLS) in consideration, we see that for sample size 10 GNL(ML) is always in the first rank (in respect of taking less time) and PHL(ML) is in the second position except the case $\theta_1 = -1.15$ and $\theta_2 = -.80$, where PHL(NLS) takes the second position and MM(ML) is either in 3rd or 4th position. But, for sample size 50 PHL(NLS) is in the first position in six sets, GNL(ML) is in the second position in six sets and first in other two, whereas PHL(ML) takes the third position in six sets. Therefore, PHL(NLS) may have considerable attention for computing efficiency in large sample, but, considering efficiency due to variance simultaneously, GNL(ML) should be preferred over the others. However, MM(ML) did not perform very well in computing efficiency.

Therefore, from the above discussions, it appears that considering all factors GNL performs better than all others. Of course this kind of conclusion has limitations in the sense that the results may be sensitive to the particular model chosen and also the X values(given) and the MA parameters considered. In conclusion, considering all aspects, this simulated experiment is able to make a suggestion that GNL is to be preferred than the others for higher order MA process in regression errors.

2.9 Specification Error:

In a variety of specification errors, one kind is about the assumption of regression error, which costs on efficiency of regression estimates very much. If the assumed process is not the true process, the variance of the estimated regression coefficient will be biased, i.e., if the true process is (let us say), MA(2) and the assumed process is MA(1) or AR(1), the regression coefficient will be inefficient. G. S. Watson (1955) found the analytical expression of the lower bound to the efficiency of the regression estimates for the special case X'X = I and in continuation to that paper Watson and Hannan (1956) apply that lower bound for various choice of true error process and assumed process.

On an experimental basis, we did a similar kind of experiment to see how good the identification criteria discussed in Section 2.3.1 (Box-Jenkins approach) works for small samples such as 10. For large samples and even for moderate size as 50 Box-Jenkins identification criteria works very well. But for small sample using ACF (autocorrelation function) and PACF (partial autocorrelation function) it is sometimes hard to detect the order and the model of the process.

Therefore, after identifying the model using the criteria discussed in Section 273.1, we apply GNL(ML) procedure for correcting the regression errors when it is MA(1) and parallel to that for AR(1) we use Beach and MacKinnon's (1978) procedure

of Maximum Likelihood and we also apply correction for MA(2), since we know the true process is MA(2). We use only two pairs of MA parameters,

$$\langle a \rangle$$
 $\langle \theta_2 \rangle = -.50$ and $\langle \theta_1 \rangle = 1.15$

b)
$$\theta_2 = -.50 \text{ and } \theta_1 = -1.15$$

and the relative efficiencies of assumed (identified) process to the true process is given below:

	$\theta_2 =50$					
	$\theta_1 = 1.15$		$\theta_1 = -1.15$			
	βο	- β1	βο	β1		
	n1 = 30		n2 = 21			
REAR1	.9318	.9143	.9908	.9580		
	n3 :	= 51	n4 =	36		
REMA 1	.8588	.8413	.9918	.9851		

From the above results we see that relative efficiency³

³ Where, the relative efficiency REAR1 is defined as the estimated variance of true process MA(2) divided by the estimated variance of identified process AR(1) for the identified number of samples n1 and n2 for two pairs of θ 's. Similarly, REMA1 is the relative efficiency defined as the estimated variance of true MA(2) process divided by the estimated variance of identified MA(1) process for the identified number of samples n3 and n4.

does not fall very much with respect to the true process, which tells us that the Box-jenkins identification criteria does not give us very poor result though it identifies the model wrongly for the number of cases mentioned in the table (i.e. the number of repetitions). But, since the results obtained only used a few cases (where it identifies the model other than MA(2)), these findings can not be very reliable and may not be justified for other cases. But the truth is that a wrongly identified model can give us a better estimate of the regression coefficient, though this is not always true.

C H A P T E R

EXACT DETERMINANT OF COVARIANCE MATRIX

3.1 Determinant of Covariance Matrix Ω

For Maximum Likelihood method the determinant of Ω plays an important role. Judge(1980,p.205) mentioned that evaluation of $|\Omega|$ is a headache in the case of ML.

There have been a number of approaches for exact maximum likelihood and also for approximate ML, but the latter one is asymptotically the former one. The approximation can arise from the approximation in transformation or from the approximation in determinant. Box and Jenkins(1976,p.213) for univariate time series suggested an approximation of the latter kind by disregarding the the determinant. McLeod(1978) proposed an approximation of the determinant term and claims a closer approximation to the exact ML. Ansley(1976,p.59) discussed the fact that approximation by disregarding the determinant can lead to inferior estimates; he gave references to different Monte Carlo works.

3.2 Determinant from the Transformation of General Procedure

Ansley use the determinant proposed by Phadke and Kedem(1978) using library subroutine: It is,

$$|\Omega| = |S'S|$$

- = |S'||S|
- = $(product of diagonal elements in S)^2$

This can be obtained from our square root matrix S discussed in Chapter 2, when we are using General Procedure, because the elements of S are already obtained for transformation. We just need to use the diagonal elements of S. Therefore, we are getting the determinant as a by-product. But, if one is not using General Procedure (GNL), then it is better to apply the technique discussed below to estimate the determinant of Ω .

3.3 Exact Determinant Using ⊕ Matrix

We know from Osborn(1976,pp.76-77) that the determinant of Ω can be written as $|R'R|=|\Omega|$

			1 1	1					
where	₽,	Å							
R =	0	0	0	• • • • • • • •	0	1			
	0	6,	0	• • • • • • •	1	0			
	•	•	•	• • • • • • • •	•	•			
	0	0	1	• • • • • • • •	Ď	0			
	0	1	0	• • • • • • • •	0	0			
	1	0	0	• • • • • • • •	0	0			
	$^{ heta}$ 1	$^{ heta}$ 2	^θ 3	• • • • • • • • •	^θ q-1	$^{ heta}$ q			
	$\theta_1^2 + \epsilon$	θ_2 θ_1 θ_2 θ_1	$\theta 1 \theta 3^{+\theta}$	4	$\theta_1\theta_{q-1}\theta_{q}$	θ ₁ θ _q			
and so on									
` `	L								

€.

More precisely, the rows of R^4 after q rows can be found as follows:

- 1. The (q+1,j)th element is the sum of θ_1 multiplied by (q,j)th element, θ_2 multiplied by (q-1,j)th element,, θ_q multiplied by (1,j)th element.
- 2. The (q+2,j)th element is the sum of θ_1 multiplied by (q+1,j)th ement, θ_2 multiplied by (q,j)th element,, θ_q multiplied by (2,j)th element.

n. The (q+n,j)th element is the sum of θ_1 multiplied by (q+n-1,j)th element, θ_2 multiplied by (q+n-2,j)th element,, θ_q multiplied by (q+n-q,j)th element.

In compact form R can be written as,

$$R = \begin{bmatrix} \mathbf{\tilde{I}} \\ .qxq \\ A' \\ nxq \end{bmatrix}$$

$$(n+q)xq$$

^{*}Instead of R, Osborn(1976) and Box & Jenkins(1970) use the notation X.

where,

$$\mathbf{T} = \begin{bmatrix}
0 & 0 & 0 & \dots & 0 & 1 \\
0 & 0 & 0 & \dots & 1 & 0 \\
\vdots & \vdots & \ddots & \ddots & \vdots & \vdots \\
1 & 0 & 0 & \dots & 0 & 0
\end{bmatrix}$$

and $A = [A_1 A_2 A_3 \dots A_k A_n]$

where, $A_{\dot{1}}$'s are column vectors, such that,

$$A_{1} = \Theta A_{0}$$

$$A_{2} = \Theta A_{1}$$

$$\vdots$$

$$A_{k} = \Theta A_{k-1}$$

$$\vdots$$

$$0$$

$$0$$

$$0$$

$$0$$

qx1

$$\Theta = \begin{bmatrix} \theta_1 & 1 & 0 & 0 & \dots & 0 \\ \theta_2 & 0 & 1 & 0 & \dots & 0 \\ \theta_3 & 0 & 0 & 1 & \dots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\ \theta_{q-1} & 0 & 0 & 0 & \dots & 1 \\ \theta_q & 0 & 0 & 0 & \dots & 0 \end{bmatrix}$$

The above 0 matrix is defined earlier (Section 2.5.2).

Now, R'R can be written as,

$$R'R = [T' A]$$

$$\begin{bmatrix} T \\ A' \end{bmatrix}$$

$$(n+q)xq$$

Where,

$$AA' = A_1A_1' + A_2A_2' + \dots + A_nA_n' = \Sigma A_iA_i'$$

or,
$$AA' = \Theta A_0 A_0' \Theta' + \Theta A_1 A_1' \Theta' + \dots + \Theta A_{n-1} A'_{n-1} \Theta'$$

$$= \Theta A_0 A_0' \Theta' + \Theta^2 A_0 A_0' (\Theta^2)' + \dots + \Theta^n A_0 A_0' (\Theta^n)' - -$$

$$= \sum_{i=1}^{n} \Theta^{i} A_{0} A_{0}' (\Theta^{i})'$$

Therefore,

$$|R'R| = |T'T+AA'|$$

$$= |I + \sum_{i=1}^{n} \Theta^{i} A_{0} A_{0}' (\Theta^{i})'|$$

$$= |I + \Sigma \Theta^{i} M1 (\Theta^{i})'|$$

where,
$$M1 = A_0 A_0' = \begin{bmatrix} 1 & 0 & 0 & \dots & 0 \\ 0 & 0 & 0 & \dots & 0 \\ 0 & 0 & 0 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & 0 \end{bmatrix}$$

we can also use ,

$$|R'R| = |I + \sum_{i=1}^{n} A_{i}A_{i}'|$$

$$i=1$$
(3.2)

where |R'R| is of order qxq.

Thus, we are reducing our work to dealing with a qxq matrix rather than a big matrix (n+q)xq, and usually the order q of the MA process is very smaller relative to n. Therefore, one can use either (3.1) or (3.2) above to get the determinant of covariance matrix. The computer program in FORTRAN to calculate the determinant is given in Appendix H.2. It is also simple in the sense that here we do not need to form the complicated matrix R.

It can be noticed that for the 1st order MA process our determinant becomes,

$$|R'R| = |1 + \sum_{i=1}^{n} \Theta^{i} M1 (\Theta^{i})'|$$

$$= \left| 1 + \sum_{i=1}^{n} \Theta^{i} (\Theta^{i})' \right|$$

$$= |1 + \sum_{i=1}^{n} \Theta^{2i}|.$$

Since Θ is a scalar and M1 is 1,

$$|R'R| = 1 + \theta^2 + \theta^4 + \dots + \theta^{2n}$$

$$1 - \theta^{2(n+1)}$$

$$1 - \theta^2$$

which was reported by Box and Jenkins(1976,P.272) and also by Balestra(1980,p.381).

CHAPTER 4

APPROXIMATE ESTIMATOR FOR THE HIGHER ORDER MOVING AVERAGE
PROCESS IN REGRESSION ERRORS

4.1 Approximate Transformations for MA Process:

Along with the exact transformations, researchers also get themselves involved with approximate transformations. It is obvious that we can get better results using exact transformation than using approximate, but the latter is asymptotically the former. Approximate transformations are used for computational simplicity. Balestra(1980.pp.390-394) proposed an approximate transformation matrix T* of dimension (n-1)xn for MA(1) and showed that the transformation can be carried out recursively as,

$$\tilde{\epsilon}_{i} = \sum_{j=1}^{i} c^{i-j} \epsilon_{j}, i \ge 2,$$

where, c is the MA parameter;

Thus, Balestra is loosing the first observation. With that in mind later Park and Heikes(1983) propose another approximate transformation P augmenting T* by a first row consisting of 1 in the 1st column and zeroes in others for the same order of MA process, where P is of order nxn.

In both the papers, they considered a simple regression equation with constant term only and they derived the analytical expression for the variance of the estimated constant using their transformation, which is reproduced here below.

Balestra

For c<1:

OLS:

$$\sigma^{2} \left[\frac{(1-c)^{2}}{n} + \frac{2c}{n^{2}} \right]$$

APX:

$$\sigma^{2}\left[\begin{array}{c} \frac{(1-c)^{2}}{n-1-2c^{2}r_{1}+c^{4}r_{2}} + \frac{(1-c)^{2}c^{4}(r_{1}-c^{2}r_{2})^{2}}{(n-1-2c^{2}r_{1}+c^{4}r_{2})^{2}} \end{array}\right]$$

where $r_1 = (1-c^{n-1})/(1-c)$, and $r_2 = (1-c^{2n-2})/(1-c^2)$.

AITKEN(GLS):

$$\sigma^{2} \frac{(1-c)^{2}}{n} \left[1 - \frac{2c(1-c)^{n}}{n(1-c)(1+c^{n+1})} \right]^{-1}$$

For c=1:

OLS:
$$\sigma^2 = \frac{2}{n^2}$$

APX:
$$\sigma^2 = \frac{3n(n^2-1)(3n+10)}{[(2n+1)(n+1)n -6]^2}$$

AITKEN(GLS): $\sigma^2 \frac{n}{n(n+1)(n+2)}$

Park and Heikes

For č≈4:

$$\sigma^{2}[\frac{1-c^{2})(1-c)^{2}}{H} + \frac{H^{2}}{H^{2}}$$
where $H = n(1-c^{2})-c(1-c^{n})(2+c-c^{n+1})$
For $c = 1$:
$$\sigma^{2}[\frac{(9n+3)(n+2)}{n(2n+1)^{2}(n+1)}]$$

where, APX stands for Approximate Transformation by Balestra (hereafter BL) and MAPX is the Modified Approximate Transformation by Parks and Heikes.

On the basis of numerical computations of relative efficiencies, for six sample sizes and six values of c, BL finds that:

- (a) OLS performs better than APX when c is low.
- (b) APX performs extremely well for c around 0.5, but does very poorly for high values of c, even in larger sample sizes.

On the other hand, Park and Heikes using their transformation observe that:

- (a) For c around 0.5, MAPX performs extremely well and better than APX for $c \le 0.5$.
- (b) Like APX, MAPX does not perform well for high values of c,

and the performance is about the same as APX for c in the interval of 0.5 to 0.99 .

From Appendix C.1 (reproduced here) it can be observed that, MAPX does better than APX for c below 0.5, but, does not perform as APX for c above 0.5.

Choudhury and Chaudhury(1984) propose another approximate transformation P of dimension nxn as below:

$$P = \begin{bmatrix}
\frac{1}{\sqrt{(1+c^2)}} & 0 & 0 & \dots & 0 \\
\frac{c}{1+c^2} & 1 & 0 & \dots & 0 \\
\frac{c^2}{1+c^2} & c & 1 & \dots & 0 \\
\vdots & \vdots & \ddots & \vdots & \vdots \\
\frac{c^{n-1}}{1+c^2} & c & c & \dots & 1
\end{bmatrix}$$

where the transformation can be carried out in a simple recursive way,

$$\widetilde{\epsilon}_1 = \epsilon_1 / \sqrt{(1+c^2)}$$

$$\widetilde{\epsilon}_2 = \epsilon_2 + \epsilon_1 c / (1+c^2)$$

 $\tilde{\epsilon}_t = \epsilon_t + c\tilde{\epsilon}_{t-1}$, t=3,...,n.

They found the variance of the estimate of constant for the same 'intercept only' model is,

$$\sigma^{2} \frac{6\{2n(4n^{2}-1)+3(n^{2}-1)^{2}+6\}}{\{n(4n^{2}-1)+3\}^{2}}$$

They also compute numerically the relative efficiency for APX, MAPX and FMAPX(Further Modified Approximate transformation) to the GLS for eight different sample sizes and six values of c in Appendix C.1, which shows that FMAPX is a better approximation in the sense that, it performs better than the previous two for all values of c and the sample sizes considered. It can be found that FMAPX performs as well as GLS for c less than 0.7. In Appendix C.2 (reproduced here), they showed the relative efficiency of APX and MAPX to FMAPX.

The approximation proposed by Park and Heikes is also discussed by Pollock(1979,pp.203-207) for MA(1) process.

Both the previous two approximations i.e., APX and MAPX uses the covariance matrix whose determinant is 1 as shown by Balestra (1980,p.390). Therefore, ML estimate for these is

equivalent to the least squares. For the FMAPX the determinant can be found as $1+c^2$. Therefore, ML estimate can be obtained by maximizing the log-likelihood,

$$L(\beta,c,\sigma^2) = \frac{n}{2} \ln \sigma^2 - \frac{1}{2} \ln (1+c^2) - \frac{1}{2\sigma^2} (\hat{Y}-\hat{X}\beta')(\hat{Y}-\hat{X}\beta)$$

using the ML estimate of σ^2 , the concentrated log-likelihood function becomes,

$$L(\beta,c) = \frac{n}{2} \ln \left[1+c^2\right]^{(1/n)} (\hat{Y}-\hat{X}\beta)'(\hat{Y}-\hat{X}\beta)$$

where, X and Y are the transformed variables.

4.2 Modified Approximate Transformation(MAPX) for Higher Order MA Process:

Unfortunately, FMAPX can not readily be generalized for higher order MA process, but MAPX can be generalized as below. Where the transformation matrix for MA(q) can be written as,

T'=
$$\begin{bmatrix} 1 & 0 & 0 & \dots & 0 \\ \theta_1 & 1 & 0 & \dots & 0 \end{bmatrix}$$

 $(\theta_1^2 + \theta_2)$ $\theta_1 & 1 & \dots & 0 \\ (\theta_1^3 + 2\theta_1\theta_2 + \theta_3)$ $(\theta_1^2 + \theta_2)$ $\theta_1 & \dots & 0 \end{bmatrix}$
and so on

This transformation matrix T is the square root matrix obtained from Vo^{-1} , where Vo^{-1} is the inverse of approximate covariance matrix Vo, which for MA(2) can be defined as below:

$$Vo = \begin{bmatrix} 1 & -\theta_1 & -\theta_2 & 0 & 0 & \dots & 0 \\ -\theta_1 & 1+\theta_1^2 & -\theta_1(1-\theta_2) & -\theta_2 & 0 & \dots & 0 \\ -\theta_2 & -\theta_1(1-\theta_2) & 1+\theta_1^2+\theta_2^2 & -\theta_1(1-\theta_2) & -\theta_2 & \dots & 0 \\ 0 & -\theta_2 & -\theta_1(1-\theta_2) & 1+\theta_1^2+\theta_2^2 & -\theta_1(1-\theta_2) & \dots & 0 \end{bmatrix}$$

Therefore, we can see that only the first four elements in the left upper corner of Vo are approximated with the corresponding elements of exact V matrix; elsewhere the elements are identical.

The above transformation matrix Υ can be obtained starting with 1's in the main diagonal and all zeroes above the main diagonal. Then the (2,1)th element is the multiplication of θ_1 with the (1,1)th element; (3,1)th element is the sum of multiplication of θ_1 with (2,1) and θ_2 with (2,2); (3,2)th element is the multiplication of θ_1 with (2,2); ...; (k,1)th element is the sum of multiplication of θ_1 with (k-1,1), θ_2 with (k-1,2),...., θ_{k-1} with (k-1,k-1)th element; similarly (k,2)th element is the sum of multiplication of θ_1 with (k-1,2), θ_2 with (k-1,3),...., θ_{k-2} with (k-1,k-1); and so on.

But, more simply, we can obtain the transformation matrix after obtaining the 1st column, because, all the diagonal elements of a diagonal on and below the main diagonal are the same. Therefore, first element of 1st row will construct main diagonal, first element of 2nd row will construct 2nd diagonal, first element of 3rd row will construct 3rd diagonal and so on. It is easy to obtain the first column recursively as follows:

- a) 1st element is 1.
- (b) 2nd element is $\theta_1(a)$.
 - c) 3rd element is $\theta_1(b) + \theta_2(a)$.

d) 4th element is $\theta_1(c) + \theta_2(b) + \theta_3(a)$.

- q) qth element is $\theta_1(q-1) + \theta_2(q-2) + ... + \theta_{q-1}(a)$.
- q+1) (q+1)th element is $\theta_1(q) + \theta_2(q-1) + \dots + \theta_q(a)$.
- q+2) (q+2)th element is $\theta_1(q+1)+\theta_2(q)+\ldots+\theta_q(b)$.
- n) nth element is $\theta_1(n-1)+\theta_2(n-2)+...+\theta_q(n-q)$.

If we want to form the transformation matrix, the above procedure is convenient, but, if our objective is only to transform the variable then the former procedure seems more convenient in respect of computer space, because, all we need to store is the previous row, to form the present row.

But, for practical purposes, we can use the recursive transformation discussed below.

Since our purpose is to transform the variable, the following super-simple recursive procedure can be adopted.

$$\hat{Y}_1 = Y_1$$

$$\dot{Y}_2 = Y_2 + \theta_1 \dot{Y}_1$$

$$\hat{Y}_3 = Y_3 + \theta_1 \hat{Y}_2 + \theta_2 \hat{Y}_1$$

 $\hat{Y}_q = Y_q + \theta_1 \hat{Y}_{q-1} + \cdots + \theta_{q-1} \hat{Y}_1$

 $\hat{Y}_{q+1} = Y_{q+1} + \theta_1 \hat{Y}_q + \dots + \theta_q \hat{Y}_1$

$$\hat{Y}_n = Y_n + \theta_1 \hat{Y}_{n-1} + \dots + \theta_q \hat{Y}_{n-q}$$

Thus, for example, for MA(2) process the transformation can be carried out as,

$$\hat{Y}_1 = Y_1$$

$$\hat{Y}_2 = Y_2 + \theta_1 \hat{Y}_1$$

$$\hat{Y}_3 = Y_3 + \theta_1 \hat{Y}_2 + \theta_2 \hat{Y}_1$$

$$\hat{Y}_4 = Y_4 + \theta_1 \hat{Y}_3 + \theta_2 \hat{Y}_2$$
.

$$\hat{\mathbf{Y}}_{n} = \mathbf{Y}_{n} + \theta_{1} \hat{\mathbf{Y}}_{n-1} + \theta_{2} \hat{\mathbf{Y}}_{n-2}$$

Therefore, if θ is unknown, using the estimated value of θ 's we can transform the variables using our above recursive transformation procedure to perform two-stage EGLS.

4.3 Empirical Results:

We have computed the relative efficiencies of MAPX and GLS to OLS 5 and also the relative efficiency of GLS to MAPX 6 for the model considered by Balestra and hence we can not generalize the results obtained, since the performance of the approximate estimator also depends on the independent variables. But from this simple model we can at least show some of the criteria of an approximate estimator. We have computed the relative efficiency numerically (presented in Appendix E.1 to Appendix E.6, Appendix F.1 to Appendix F.6 and Appendix G.1 to Appendix G.6) for the pairs of θ 's as below:

$$-1.90 \le \theta_1 \le 1.90$$

$$-0.95 \le \theta_2 \le 0.95$$

both with an increment of 0.10 and also,

$$\theta_2 + \theta_1 \leq 0.95$$

$$\theta_2 - \theta_1 \leq 0.95$$

The expression for the variances of the estimated constant are given below:

OLS:
$$\sigma^2 (X'X)^{-1} X'VX (X'X)^{-1}$$
 (see Johnston p.246)

⁵i.e., the variance of regression coefficient obtained by MAPX is divided by the variance obtained by OLS, and the variance of GLS divided by the variance of OLS.

Si.e., the variance of GLS divided by the variance of MAPX.

$$\sigma^{2} \overset{n}{\Sigma} \overset{n}{\Sigma} \overset{n}{V}_{ij}$$

$$i=1 \ j=1$$

$$= \frac{1}{n^{2}} \qquad , \ n \ is \ the \ sample \ size.$$

$$m^{2}$$

$$MAPX: \sigma^{2} (X'Vo^{-1}X)^{-1} X'Vo^{-1}V Vo^{-1}X (X'Vo^{-1}X)^{-1}$$

$$= \sigma^{2} (\mathring{X}'\mathring{X})^{-1} \mathring{X}' (TVT')\mathring{X} (\mathring{X}'\mathring{X})^{-1}$$

where, $\mathbf{\hat{x}}$ is the transformed observations using the approximate transformation and Vo^{-1} is the inverse of the approximate Vo matrix which is defined above.

GLŚ:
$$\sigma^2 (X'V^{-1}X)^{-1}$$

= $\sigma^2 (X'X)^{-1}$

where, X is the exact transformation using the transformation matrix S discussed in Chapter 2.

From the results presented in Appendix F.1 to Appendix F.6 for six different sample sizes, we observe that,

- a) MAPX does extremely well with respect to OLS when θ_1 and θ_2 both are positive and sample size is greater than 10; for sample size 10 or less its performance is not very good.
- b) For the region of θ_2 in between -0.55 and 0.0 (inclusive), with positive θ_1 its performance is very good for all sample sizes considered and as sample size increases the performance is excellent, specifically for higher values of θ_1 . For negative θ_1 it does not perform very well except for the couple of points in the region ,

$$-.60 \le \theta_1 \le 0.0$$

$$-.35 \le \theta_2 \le 0.35$$

c) Again its performance can be appreciated in the (tables, i.e. Appendix F.1 to Appendix F.6) lower triangle of the reactangle bounded by the region,

$$0.0 \le \theta_1 \le 1.90$$

$$-.95 \le \theta_2 < -.55$$

for sample sizes greater than 10 and for size 10 or less the performance is reasonable.

Compared with GLS, the approximate estimator does well (middle of the Appendix G.1 to Appendix G.6) and as the sample size increases the performance increases too. If we compare Appendix G.1 and Appendix G.6, we see that in the middle of tables the number of ones (1.000) increases in substantial amount. Again comparing Appendix G.5(n=50) and Appendix G.6(n=100) the improvement of approximate estimator can be observed very clearly, specifically the lower part of the table, i.e., when both θ 's are positive. Therefore, for negative θ 's it is not doing very well.

As we said before, for the region, $-.30 \le \theta_1 \le 0.30$

$$-.25 \le \theta_2 \le 0.25$$

(i,e, in the middle of the tables) there is no reason not to consider approximate estimator rather than exact (GLS) on the ground of computational simplicity and the above region of θ 's becomes increases as sample size gets larger.

Thus, we can say that the approximate estimator does as well as exact for small values of θ 's and can also be considered for large θ 's when sample size is larger.

From Appendix E.1 to Appendix E.6, it is observed that OLS does worse with respect to GLS in the bottom line of the tables (i,e, for the highest values of θ_1 , for each θ_2) but does well in the middle of tables, where both θ 's are near to zero, which means there is virtually no moving average effect and hence GLS merges to OLS. Another important aspect is that, as both the θ 's tends to zero from both ends efficiency gain by GLS over OLS diminishes.

As we discussed in the previous Chapter, for high values of θ_1 (for intercept) efficiency gain over OLS is higher than for low values of θ_1 ; this can be reconfirmed from Appendix E.1 to Appendix E.6 and also it is to be observed that when the sign of θ_1 is positive (with high Value of θ_1) efficiency gain is much more than with negative θ_1 , which verifies our previous result.

C H A P T E R 5

CONCLUSION

It is apparent from the results of simulation experiment from Appendix A.1 to Appendix A.8 that the General Procedure (GNL) performs better than the other two procedure for both sample sizes considered. It performs excellently for sample size 10. We have compared the relative efficiency of the estimated regression coefficient for a simple regression model with an intercept and a slope coefficient. The relative efficiency is defined as the estimated variance of the regression coefficient by OLS divided by the estimated variance of regression coefficient by three different procedures obtained from 100 repetitions. The results obtained are reported in Appendix A.1 to Appendix A.8, which are further analysed using analysis of covariance and the findings are reported in Appendix B.1 to Appendix B.6. It can be observed from Appendix A.1 to Appendix A.4, for sample size 10, that the General procedure(GNL) performs very well over the others. Which can easily be understood from Appendix B.3 (sample size 10) that the proposed transformation GNL(ML) does better than the others.

The efficiency due to computational time, i.e., the time required by the central processing unit (cpu) in the computer is reported in Appendix A.1 to Appendix A.8 and it is observed that GNL(ML) takes always less time than the other two for both the sample sizes considered.

In Chapter 3 we have shown the determinant for covariance matrix can be obtained as a by-product when General Procedure (GNL) is in consideration. We also have shown in details how an exact determinant can be obtained. It can be observed that the dimension of the matrix for which the determinant is to be calculated is reduced from (n+q)xq to qxq, which reduces our work and makes the computational effort much simpler. Because, the order of the moving average process q is very much smaller than the number of observations n, we have in practice.

Therefore, one can use this exact determinant for any of the three procedures discussed in Chapter 2. Specifically, it is important to use this determinant when one is using MacDonald and MacKinnon Procedure or Phillips Procedure. Because, they do not have any determinant to be obtain as a by-product like General Procedure.

In Chapter 4, we have discussed the efficiency of proposed approximate estimator relative to the GLS and OLS. We have computed the relative efficiency for six different sample sizes. The results are tabulated from Appendix E.1 to Appendix E.6 for relative efficiency of GLS to OLS, from Appendix F.1 to Appendix F.6 for relative efficiency of MAPX to OLS and from Appendix G.1 to Appendix G.6 for relative efficiency of GLS to MAPX. It is to be observed from Appendix G.1 to Appendix G.6 that approximate estimstor performs as well as exact estimator in the middle of the tables, i.e., when both the moving average parameters are small in magnitude. As sample size increases, i.e., as we move

from Appendix G.1 to Appendix G.6 the efficiency of the approximate estimator increases. Therefore, in that region of the MA parameters, i.e., in the middle of the tables the approximate transformation may be considered instead of exact transformation on the ground of computational simplicity.

REL. EFFICIENCY AND BIAS OF BO AND B1 ESTIMATES WITH RESPECT TO OLS									
,	e	EG	LS		ML				
n = 10	Во		В	1	В	0	В1		
	Eff.	Bias.	Eff.	Bias	Eff.	Bias	Eff.	Bias	
GNL:	1.663	0.104	1.548	056	1.734	0.038	1.616	021	
MM:	1.449	0.068	1.316	033	1.607	006	1.469	.007	
PHL:(NLS)	1.770	0.124	1.582	072	1.709	0.028	1.592	017	

$\theta_1 = 1.45$	CPU GNL(ml)	TIME: (in MM(ml)	milliseconds) PHL(ml)	PHL(nls)
$\theta_2 =50$	280.3	526.0	397.9	749.0

REL. EFFICIENCY AND BIAS OF BO AND B1 ESTIMATES WITH RESPECT TO OLS									
EGLS ML							ĪĹ		
n = 10	Во		В	1		Во	В1	·	
	Eff.	Bias	Eff.	Bias	Eff.	Bias	Eff.	Bias	
GNL:	1.562	169	2.162	0.034	1.763	115	2.821	0.006	
MM:	1.260	195	1.585	0.012	1.344	133	1.641	022	
PHL: (NLS)	1.535	089	1.912	003	1.748	128	2.734	0.011	

$\theta_1 = -1.45$	CPU GNL(ml)	TIME:(in MM(ml)	milliseconds PHL(ml)) PHL(nls)
$\theta_2 =50$	166.3	519.0	288.7	557.0

APPENDIX A.2

REL. EFFICIENCY AND BIAS OF BO AND B1 ESTIMATES WITH RESPECT TO OLS									
	EGLS					ML			
n = 10	B	0	B1		Bo		B 1		
	Eff.	Bias	Eff.	Bias	Eff.	Bias	Eff.	Bias	
GNL:	1.914	0.030	1.783	025	2.218	0.023	2.103	022	
MM:	1.688	0.019	1.510	020	2.188	039	2.004	0.012	
PHL: (NLS)	2.325	0.036	2.173	028	2.234	0.022	2.116	022	
	l <u>.</u>							,	

$\theta_1 = 1.15$	CPU T GNL(ml)		milliseconds) PHL(ml)	
$\theta_2 =50$	280.8	520.0	. 383.0	545.0

REL. EFFICIENCY AND BIAS OF BO AND B1 ESTIMATES WITH RESPECT TO OLS									
EGLS						M	IL ,	<u> </u>	
n = 10	Во	Во		B1 B0		Во	B1		
	Eff.	Bias	Eff.	Bias	Eff.	Bias	Eff.	Bias	
GNL:	1.525	178	1.863	0.043	1.520	139	2.136	0.024	
MM:	1.140	157	1.170	006	1.196	138	1.133	007	
PHL:(NLS)	1.329	096	1.560	0.001	1.544	131	2.168	0.022	

$\theta_1 = -1.15$	CPU GNL(ml)	TIME:(in MM(ml)	milliseconds) PHL(ml)	PHL(nls)
$\theta_2 =50$	166.3	541.0	295.0	434.0

APPENDIX A.3

REL. EFFICIENCY AND BIAS OF BO AND B1 ESTIMATES WITH RESPECT TO OLS									
		EG	LS	 	ML				
n = 10	Bo B1		1	Во		B 1			
	Eff.	Bias	Eff.	Bias	Eff.	Bias	Eff.	Bias	
GNL:	2.113	0.080	1.958	050	3.217	0.023	2.933	020	
MM:	1.941	0.065	1.772	044	2.604	0.018	2.359	018	
PHL:(NLS)	2.940	0.071	2.621	046	3.217	0.023	2.933	020	

$\theta_1 = 1.45$	CPU T GNL(ml)		illiseconds PHL(ml)	
θ₂ =80	280.5	491.0	380.5	430.0

REL. EFFICIENCY AND BIAS OF BO AND B1 ESTIMATES WITH RESPECT TO OLS									
		EG	LS	•	ML				
n = 10	Во	·-··	B1		Во		B1		
	Eff.	Bias	Eff.	Bias	Eff.	Bias	Eff.	Bias	
GNL:	1.528	173	2.422	0.027	1.707	144	3,927	0.019	
MM:	1.161	139	1.488	027	1.398	116	1.525	036	
PHL: (NLS)	1.506	074	1.959	020	1.702	136	3.449	0.009	

$\theta_1 = -1.45$			milliseconds) PHL(ml)	
$\theta_2 =80$	156.3	455.0	298.0	415.0

1	REL. EF		Y AND E		Bo AND O OLS	B1 ESTI	MATES	
<u> </u>		EGL	S		ML			
n = 10	Во		E	B1 .		Во		
	Eff.	Bias	Eff.	Bias	Eff.	Bias	Eff.	Bias
GNL:	2.246	006	2.214	013	3.042	009	3.136	012
MM:	1.740	0.003	1.535	021	2.169	0.017	1.979	030
PHL:(NLS)	2.763	0.018	2.829	023	3.042	009	3.136	012

I	REL. EFFICIENCY AND BIAS OF BO AND B1 ESTIMATES WITH RESPECT TO OLS										
	ML										
n = 10	Во		- B1		Во		B1				
	Eff.	Bias	Eff.	Bias	Eff.	Bias	Eff.	Bias			
GNL:	1.364	169	1.747	0.033	1.427	191	1.979	0.046			
MM:	1.002	116	0.824	044	0.983	119	0.702	054			
PHL:(NLS)	1.282	155	1.613	0.024	1.402	186	1.900	0.042			

$\theta_1 = -1.15$	CPU GNL(ml)		milliseconds) PHL(ml)	
$\theta_2 =80$	153.5	472.0	416.0	255.0

REL. EFFICIENCY AND BIAS OF BO AND B1 ESTIMATES WITH RESPECT TO OLS										
EGLS]	ML	₹.		
n = 50	n = 50 Bo			1	Bo (B)		B1			
	Eff.	Bias	Eff.	Bias	Eff.	Bias	Eff.	Bias		
GNL:	13.086	022	12.652	0.011	25.057	012	23.850	0.007		
MM:	13.008	021	12.592	0.011	27.229	007	27.350	0.004		
PHL:(NLS)	22.786	0.017	22.416	007	31.123	008	30.664	0.005		

$\theta_1 = 1.45$	CPU T GNL(ml)	'IME:(in mi MM(ml)	lliseconds PHL(ml)	
$\theta_2 =50$	1807.0	3675.0	2581.0	2653.0

REL. EF	FICIEN				B1 EST	IMATES				
EGLS						ML				
БО ВО		В	<u>, </u>	Во		B1				
Eff.	Bias	Eff.	Bias	Eff.	Bias	Eff.	Bias			
1.841	0.005	12.632	0.014	1.861	0.030	47.952	0.003			
1.768	000	11.627	0.014	1.819	0.025	47.362	0.004			
1.470	0.096	39.547	0.004	1.880	0.029	47.878	0.004			
	Bo Eff. 1.841	Bo Eff. Bias 1.841 0.005 1.768000	BO E Eff. Bias Eff. 1.841 0.005 12.632 1.768000 11.627	EGLS BO B1 Eff. Bias Eff. Bias 1.841 0.005 12.632 0.014 1.768000 11.627 0.014	### RESPECT TO OLS Figure	WITH RESPECT TO OLS EGLS I Bo B1 B0 Eff. Bias Eff. Bias Eff. Bias 1.841 0.005 12.632 0.014 1.861 0.030 1.768 000 11.627 0.014 1.819 0.025	WITH RESPECT TO OLS EGLS			

$\theta_1 = -1.45$	GNL(ml)	TIME: (in mi MM(ml)	lliseconds PHL(ml)	
$\theta_2 =50$	1037.0	2188.0	1369.0	2400.0

REL. EFFICIENCY AND BIAS OF BO AND BI ESTIMATES WITH RESPECT TO OLS EGLS ML										
	ML									
n = 50	n = 50 Bo			1	Bo B1		B 1			
	Eff.	Bias	Eff.	Bias	Eff.	Bias	Eff.	Bias		
GNL:	5.302	032	4.881	0.017	4.579	020	4.358	0.011		
MM:	5.178	032	4.768	0.018	4.386	023	4.189	0.013		
PHL: (NLS)	3.938	018	3.800	0.011	4.416	026	4.257	0.014		

$\theta_1 = 1.15$	CPU T	IME:(in mi MM(ml)	lliseconds PHL(ml)	
$\theta_2 =50$	1037.0	1841.0	1211.0	917.0

,	REL. EFFICIENCY AND BIAS OF BO AND B1 ESTIMATES WITH RESPECT TO OLS										
	,	EGL	S		ML						
n = 50	Во		В	B 1		Во		T.			
	Eff.	Bias	Eff.	Bias	Eff.	Bias	Eff.	Bias			
GNL:	1.477	012	3.830	0.020	1.480	010	4.863	0.020			
MM:	1.442	0+3	3.609	0.016	1.466	012	4.70	0.015			
PHL: (NLS)	1.442	008	4.464	0.021	1.480	016	A.863	0.020			

θ1	=-1.15	CPU GNL(ml)	J TIME:(in MM(ml)	millisecond PHL(ml)	s) PHL(nls)
θ 2	=50	377.0	800.0	505.0	353.0

,	REL. EFFICIENCY AND BIAS OF BO AND BI ESTIMATES WITH RESPECT TO OLS										
· .		EGL	ıS				MY	-			
n = 50	Во	· 	В	1		Во	. B1	,			
· + 3	Éff.	Bias	Eff.	Bias	Eff.	Bias	Eff.	Bias			
GNL:	10.167	005	9.311	Q.004	13.175	007	12.823	0.005			
MM:	9 609	005	8.985	0.004	13.596	004	14.060	0.004			
PHL:(NLS)	13.488	007	13.128	0.005	14.746	006	14.732	0.004			

$\theta_1 = 1.45$,	CPU GNL(ml)	TIME:(in m	illiseconds PHL(ml)) PHL(nls)
$\theta_2 = .80$	* \$	1002.0	1485.0	1224.0	476.0

REL! EFFICIENCY AND BIAS OF BO AND BI ESTIMATES WITH RESPECT TO OLS								
	is a second	EG	LS		<i>V</i>	ì	ML ,	
n = 50	Во	,	В	1		Во	В1	
	Eff.	Bias	Eff.	Bias	Eff.	Bias	Eff.	Bias
GNL:	1.816	0.003	9.526	0.016	1.703	0.008	12.167	0.014
MM:	1.784	0.006	8.482	0.010	1.618	0.011	10.734	0.009
PHL:(NLS)	1.675	0.015	12.463	0.011	1.692	0.010	12.559	0.013

θ 1	=-1.45	CPU GNL(ml)		milliseconds) PHL(ml)		
θ 2	=80	451.0	999.0	806.0	2:6.4	-

REL. EFFICIENCY AND BIAS OF BO AND BI ESTIMATES WITH RESPECT TO OLS EGLS ML Bo B1 n = 50Во Eff. Bias Eff. Bias Eff. Bias Eff. Bias 0.001 5.829 -.016 5.710 0.011 7.667 7.755 0.003 GNL: 5.746 -.018 5.448 0.012 6.816 MM: 6.824 0.010 -.002 PHL: (NLS) 5.620 0.014 5.547 -.003 7.167 0.004 7.101 0.001

 $\theta_1 = 1.15$ CPU TIME: (in milliseconds)
GNL(ml) MM(ml) PHL(ml) PHL(nls) $\theta_2 = -.80$ 716.0 1576.0 1310.0 371.0

]	REL. EFFICIENCY AND BIAS OF BO AND BI ESTIMATES WITH RESPECT TO OLS									
		EG		. *	. M	IL _				
n = .50	Во	Bo . B				Во	B1			
	Eff.	Bias	Eff.	Bias	Eff.	Bias	Eff.	Bias		
GNL:	1.448	015	5.382	0.024	1.446	0.023	9.125	0.006		
MM:	1.415	018	4.934	0.021	1.379	0.019	8.270	0.003		
PHL:(NLS)	1.444	0.029	8.487	0.002	1.436	0.025	8.960	0.005		

5

APPENDIX B.1
(ANOCOVA)
(combined samples)

ANALYSIS OF VA	ARIANCE OF REL.	EFFICIENCY O	F Во
SOURCE DF REGRESSION 9 FIRST 5 VARS 5 ERROR 86 TOTAL 95	1477.8 164 40.081 8.0	N SQR F-STAT .20 8.6434 162 .42198 997	SIGNIF .0000 .8322
VARIABLE COEFF CONSTANT -10.645 -101.T1731 102.T2 .439 103.T3953 104.T4 .327 105.T5 .460 106.T6 .873 5.SMSZ .117 6.TH2 2.743 7.STH1 2.657 8.MTH1 10.061	4.3843 .9947 .9947 .9947 .9947 .9947 .9947 .2224 -1 2.9656 .4448	-2.42797349 .44109580 .3285 .4621 -1 .8772 5.2580 .9248 5.9720	GNIF .0173 .4644 .6603 .3408 .7433 .9632 .3828 .0000 .3577 .0000

ANALYSI	S OF VAR	IANCE OF RE	L. EFFICIE	NCY of B1
SOURCE REGRESSION FIRST 5 VAI ERROR TOTAL	DF 9 RS 5 86 95	4680.1 360.51	MEAN SQR 520.01 72.101 53.249	F-STAT SIGNIF 9.7655 .0000 1.3540 .2497
VARIABLE	COEFF	STD ERRO	R T-STAT	SIGNIF
, 101.T1	-24.740 -2.402 1.593 -2.900	7.3404 1.6654 1.6654 1.6654	-3.3704 -1.4422 .9568 -1.7415	.1529
104.T4 105.T5 106.T6 5.SMSZ	1.143 .503 2.062 .268	1.6654 1.6654 1.6654 .3724	.6866 .3022 1.2382	.7632
6.TH2 7.STH1 8.MTH1	10.931 765 23.982	4.9651 .7448 4.9651	2.2015 -1.0277 4.8300	.0304

APPENDIX B.2

(ANOCOVA) (combined samples)

		<u> </u>		
# * I	ANALYSIS OF V	VARIANCE OF	BIAS OF BO	o '
SOURCE		SQRS MEAN	SQR F-S	STAT SIGNIF
REGRESSION	9 .2037	,2264	11 -1 17.2	.0000
FIRST 5 V	ARS 5 .3773	30 -2 .7546	51 -3 .57	410 .7196
ERROR	86 .1130)4 .`1314	14 - 2	
TOTAL	95 .3168	31 -		
ſ	•			
VARIABLE	COEFF	STD ERROR	T-STAT	SIGNIF
Ç,A ^r	•			•
CONSTANT	.10420	.36469 -1	2.8573	.0054
101.T1	.11240 -1	.82740 -2	1.3584	.1779
102.T2	27542 -2	.82740 -2	3329	.7400
103.T3	.232712	.82740 -2	.2813	.7792
104.T4	89417 -2	.82740 -2	-1.0807	.2829
105.T5	.17833 -2	.82740 -2	.2155	.8299
106.T6	36542 -2	.82740 -2	4416	.6599
5.SMSZ	18224 -2	.18501 -3	-9.8501	.0000
6.TH2	.24625 -1	.24668 -1	.9982	.3210
7.STH1	27137 -1	.37003 -2	-7.3340	.0000
8.MTH1	.14528 -1	.24668 -1	.5889	.5575
•				• • • • •

	ANALYSIS (OF VARIAN	CE OF	BIAS OF	B1	
SOURCE	DF	SUM SQRS	MEA	N SQR	F-STAT	SIGNIE
REGRESSIC	.1 9	.71467 -	2 .79	9408 - 3	5.8421	.0000
FIRST 5	VARS 5	.13378 -	2 .26	5756 -3	1.9684	.0914
ERROR	86	.11690 -	1 .13	3592 -3		•
TOTAL	95	.18836 -	1			
VARIABLE	COEFF	STD E	RROR	T-STAT	SIGN	NIF
CONSTANT	.31487	-1 .117	28 -1	2.684	19	.0087
101.T1	.72198	-2 .266	07 -2	2.713	35	.0080
102.T2	26365	· -	07 -2	990	88	.3245
103.T3	.18635		07 -2	.700	39	.4856
104.T4	25740	-2 .266		967	•	.3361
105.T5	73958		07 -2		796 -1	.9779
106.T6	37990		07 -2	-1.427		.1570
5.SMSZ			95 -4	-6.479	-	.0000
6.TH2	50764		27 -2	639	ف ا	.5239
7.STH1	26771		99 -2			.8225
8.MTH1	43403	-2 .793	27 -2	547	714	.5857

APPENDIX B.3

(ANOCOVA) (Sample Size = 10)

ANALYSIS OF V	ARIANCE OF R	REL. EFFICIE	NCY OF BO
SOURCE DF REGRESSION 8 FIRST 5 VARS 5 ERROR 39 TOTAL 47	11.817 2.6112 4.2792	1.4771	F-STAT SIGNIF 13.462 .0000 4.7597 .0017
VARIABLE COEFF CONSTANT .98063 101.T182729 102.T2 .25640 103.T339948 104.T413598 105.T5 .10915 106.T6 .25265 6.TH2 -1.04600 7.STH1 .40844 8.MTH1 .12431	.46573 .10691 .10691 .10691 .10691 .10691 .31874 .47811	2.1056 7738 2.3983 -3.7367 -1.2719 1.0209 2.3632	SIGNIF .0417 .4437 .0214 .0006 .2109 .3136 .0232 .0022 .0000 .6987

١.		~=			===		533.635	-54
	ANALYSIS	OF V	AKTAN	CE OF	REL"	EFFICI.	ENCA OF	BI
١.			10	·			_4'	
	SOURCE	DF	SUM	SQRS	MEA	N SQR	F-STAT	SIGNIF
l	REGRESSION	8	11.	726	1.40	658 🥻	6.4164	.0000
	FIRST 5 VARS	5	₹8.8	933	1.7		7.7860	.0000
	ERROR 5			0.93	.228	844		
ĺ	TOTAL	47	, 3'	635	3			
1.		-		#	34			
•	VARIABLE CO	OEFF		TD ERR	OR	T-STAT	SIG	TIV
	VARTADDE			1 D D T T T T T T T T T T T T T T T T T	.O.R.	1 51111	510.	
	CONSTANT .9	3514	- 1	.57201		.13916	.80	900
		1146		§15426		33156		420 `
Ì				•	1.			
		6810	٠, .	.15426		3.6828		007
	L .	1327		.15426		3.9756		003
ĺ	•	1177		.15426		2.6693		110
	105.T5 .1	7854	-1	.15426		.11574	.90	085
İ	106°.T6 .4°	9023		.15426	, ,	3.17790	.00	029
	6.TH2 -1.2	837		.45991	-:	2.7913	.00	081
		9104		.68987		1.1467	.2	585
		3486	-	.45991		1.8153		772
,		0 2 0 0					•	
Ι.								

(ANOCOVA) (Sample Size = 10)

	ANALYSIS (OF VARIANCE	OF BIAS OF	Во
SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT SIGNIE
REGRESSION	1 8	.14085	.17607 -1	17.945 .0000
FIRST.5 V	ARS 5	.7846 <u>8</u> -2	.15694 -2	1.5995 .1831
ERROR	39	.38265 -1	.98115 -3	
TOTAL	47	.17912	3	•
VARIABLE	COEFF	STD ERRO	OR T-STAT	SIGNIF
CONSTANT	.55708	-1 .44041	-1 1.2649	.2134
101.T1	.24692	-1 .10110	-1 2.4424	.0192
102.T2	34⁄208	-2 .10110	= 133838	.7369
103.T3	.64667	-2 .10110	-1 .63966	.5261
104.T4	15633	-1 .10110	-1 -1.5464	.1301
105.T5	60583	-2 .1011 <u>0</u>	-159927	
106.T6	60458	,	-159803	
6.TH2	.19778		-	5156
7.STH1	52287		-2°-11.565	
8.MTH1	.35389	-1 .30141	-1 1.1741	.2475
			*	

	ANALYSIS (F VARIANCE	OF BIAS OF	? B1	_
SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT SIGNI	F
REGRESSIO	N 8	.19637 -2	.24547 -3	1.0281 .431	9
FIRST 5	VARS 5	.12370 -2	.24739 -3	1.0362 .410	2
ERROR	39	.93114 -2	.23875 -3		
TOTAL	47	.11275 -1		•	
VARIABLE	COEFF	STD ERRO	OR T-STAT	SIGNIF	
CONSTANT			-1 .1248	.9013	
101.T1			-2 1.9496		
102.T2	40646		-28150	.4200	
103.T3	•		-2 .1024		
104.T4			-24040		
105.T5	.18354	-2 .49870	-2 .3680	.7148	
106.T6	59896		-2 -1.2010	.2370	
6.TH2			-1 -1.5422		
7.STH1			-2 .7127		
8.MTH1	.59028	-2 .14868	-1 .3970	.6935	

APPENDIX B.5

(ANOCOVA) (Sample Size = 50)

ANALYS	IS OF VAI	RIANCE OF	REL. EFFI	CIENCY OF	Во
SOURCE REGRESSION FIRST 5 VA ERROR TOTAL	DF 8 ARS 5 39 47	SUM, SQRS 1692.1 59.265 878.10 2570.2	MEAN SQF 211.51 11.853 22.515	F-STAT 9.3942 .52644	.0000
VARIABLE CONSTANT 101.T1 102.T2 103.T3 104.T4 105.T5 106.T6 6.TH2 7.STH1 8.MTH1	COEFF -15.253 -1.379 .621 -1.506 .790172 1.492 6.531 4.905 19.999	STD EI 6.67 1.53 1.53 1.53 1.53 1.53 4.56	15 -2.2 159 159 159 151 151 151 151	2863 9007 1054 9836 1155 1123 -1 9745 1304	GNIF 0278 3733 6874 3314 6091 9911 3358 1606 0000 0001

ANALY	SIS OF VAI	RIANCE OF REL.	EFFICIEN	CY OF 1	B 1 :
SOURCE REGRESSIO FIRST 5		~	.53 6	-STAT .5982 .7646	SIGNIF *.0000
ERROR TOTAL	39	2751.6 70. 6475.9	,	*,	
VARIABLE	COEFF	STD ERROR	T-STAT	SIG	NIF
CONSTANT	-33.479 -4.752	11.810° 2.710	-2.8348 -1.7530		072 875
102.T2 103.T3	2.619 -5.187	2.711 2.711	.9660 -1.9134		400 631
104.T4 105.T5	2.699 .989	2.711 2.711	.9953 .3647	. 7	257 173
106.T6 6.TH2	3.634 23.146	2.711 8.083	1.3404	.0	B79 067 <i>/</i>
7.STH1 8.MTH1		1.212 8.083	-1.3278 5.8309		920 / /

(ANOCOVA) (Sample Size = 50)

ANALYSIS	OF VARIANCE	OF BIAS OF	Во
SOURCE DE	SUM SQRS	MEAN SQR	F-STAT SIGNIF
REGRESSION	3 .20657 -2	.25821 -3	1.2442 .3003
FIRST 5 VARS 5	.89468 -3	.17894 -3	.86219 .5151
ERROR 39	.80940 -2	.20754 -3	
TOTAL 47	10160 -1	*	
	- i		
VARIABLE GOEF	F STD ERRO	OR T-STAT	SIGNIF
CONSTANT .4335	53 -1 .20255	-1 2.1403	.0386
101.T1 - 2212		-24759	· ·
102.T2 - 2087		-24490	
103.T31812	-	-23898	
104.T42250	-	-24839	
105.T5 .9625	\ <u>~</u>	-2 2.0701	.0451
106.T61262			
6.TH2 .2947		-1 2. 9261	.0399
7.STH1 e1987	5 -2 .20794	-2 - 9558	.3450
8.MTH16333	33 -2 .13862		.6503
•		with the	· · · · · · · · · · · · · · · · · · ·

AN	ALYSIS C	F VARIANCE	OF BIAS OF	B 1
SOURCE REGRESSION FIRST 5 VA ERROR TOTAL	DF 8 RS 5 39 47	SUM SQRS .10259 -2 .40314 -3 .82947 -3 .18554 -2	MEAN SQR .12824 -3 .80627 -4 .21269 -4	F-STAT SIGNIF 6.0295 .0000 3.7909 .0068
VARIABLE	COEFF	STD ERRO	OR T-STAT	SIGNIF
CONSTANT 101.T1 102.T2 103.T3 104.T4 105.T5 106.T6 6.TH2 7.STH1 8.MTH1	.47167 12083	1 -2 .14884 1 -2 .14884 2 -2 .14884 3 -2 .14884 3 -2 .14884 3 -1 .4437 0 -2 .6656	2 -2 5.7270 4 -2 3.1689 4 -28118 4 -2 2.1611 4 -2 -2.1051 4 -2 -1.3325 4 -2 -1.0805 7 -2 2.8794 5 -3 -3.1924 7 -2 -3.2862	0030 .4218 .0369 .0418 .1904 .2865 .0064 .0028

The ratios of the variance of AITKEN to the variances of APX, MAPX and FMAPX. For a given sample size, the first row is for APX, the second for MAPX, and the third for FMAPX.

n/c	.10	.30	.50	.70	.90	.99
3	0.712	0.812	0.921	0.988	0.944	0.895
	1/.000	0.998	0.981	0.926	0.834	0.789
	1.000	1.000	0.999	0.993	0.971	0.955
5	0.833	0.902	0.971	0.970	0.786	0.678
	1.000	0.998	0.981	0.899	0.715	0.626
	1.000	1.000	0.999	0.985	0.921	0.872
10	0.918	0.956	0.989	0.959	0.614	0.423
	1.000	0.999	0.989	0.914	0.583	0.411
	1.000	1.000	0.999	0.983	0.817	0.663
15	0.946	0.971	0.993	0.968	0.570	0.313
	1.000	0.999	0.993	0.938	0.550	0.308
	1.000	1.009	1.000	0.987	0.776	0.527
20	0.960	0.979	0.995	0.976	0.569	0.251
	1.000	1.000	0.994	0.953	0.553	0.249
	1.000	1.000	1.000	0.990	0.769	0.440
30	0.973	0.986	0.997	0.984	0.612	0.185
	1.000	1.000	0.996	0.969	0:600	0.184
	1.000	1.000	1.000	0.993	0.794	0.335
50	0.984	0.992	0.998	0.990	0.714	0.129
	1.000	1.000	0.998	0.981	0.704	0.128
	1.000	1.000	1.000	0.996	0.857	0.240
100	0.992	0.996	0.999	0.995	0.841	0.089
	1.000	1.000	0.999	0.991	0.835	0.039
	1.000	1.000	1.000	0.998	0.927	0.168

Ratios of the variance of FMAPX to the variances of APX and MAPX. The first row is for APX, and the second for MAPX.

		ď					
7	n/c.	.10	.30	.50	.70	.90	.99
*	3	0.712	0.812	0.921 0.981	0.996 0.932	0.973 0.859	0.938 0.826
	5	0.833 1.000	0.902 0.998	0.972 0.982	0.985 0.913	0.853	0.777 0.718
	10	0.918	0.956 0.999	0.990 0.990	0.976	0.752	0.638
	15	0.946	0.971 0.999	0.994 0.993	0.981 0.950	0.735 0.709	0.593 0.584
	20	0.960 1.000	0.979 1.000	0.995 0.995	0.985 0.962	0.740 0.720	0.572 0.566
	30	0.973	0.986 1.000	0.997	0.990 0.975	0.771 0.755	0.551 0.548
	50	0.984 1.000	0.992	0.998	0.994 0.985	0.831	0.536 0.535
	100	0.992	0.996	0.999	0.997 0.993	0.908	0.527 0.526

1 2 1 1 1 1 1 1 1 1					97	
HEIALT - 98 - 75 - 75 - 75 - 75 - 75 - 75 - 75 - 7		i		1	0	
THETA-1 - 95 - 85 - 75 - 65 - 55 - 45 - 25 - 15 - 25 - 15 - 25 - 15 - 25 - 15 - 25 - 15 - 25 - 2	,				, ~	
HEIA-1 - 95 - 85 - 75 - 65 - 65 - 45 - 75 - 75 - 75 - 75 - 75 - 75 - 7	7					
HITA-1 - 155 - 185 - 175 - 165 - 15					\downarrow 000	
HITH A-2 96 -85 - 75 - 65 - 75 - 45 - 35 - 35 - 35 - 35 - 35 - 35 - 3					\P	
HITH A-2 96 -85 - 75 - 65 - 75 - 45 - 35 - 35 - 35 - 35 - 35 - 35 - 3				'	υ- <u>υ</u> - υ	
HITH-1 - 56 - 165 - 75 65 65 15 15 05 - 15 - 75 - 15 05 - 15 - 75 - 15 05 - 15 05 - 15 05 - 15 05 - 15 05 - 15 05 - 15 05 - 15 05 - 15 05 05 15 05 - 05 -				,,,		
HITH-1 - 95 - 165 - 75 - 65 - 35 - 45 - 35 - 15 - 15 - 05 - 05 - 15 - 35 - 35 - 35 - 35 - 35 - 35 - 3					00000	
THETA-1 THETA-2 THETA-3 THE					0000000	
HETALTIVE EFFICIENCY OF GLS 10 QuS. HETALTIVE E					3, 3, 3, 3, 3, 3, 3, 3, 3, 3, 3, 3, 3, 3	
HEITH-1		,		4		
HITH 1-1 RELATIVE FFTCIENCY OF GLS 10 0LS HETATA HE					44444600	
HETA-1 - 26 - 85 - 75656545351505 .05 .15 .25 .35 .45 HETA-2 190. 0 882 0 849 0 859 0 859 0 879 0 8					t e e e e e e e e e e e e e e e e e e e	•
HETA-1 190. 0 682		-			23.5 8 8 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	
HETA-1 - 35 - 85 - 75 - 65 - 55 - 45 - 35 - 15 - 15 - 15 - 15 - 15 - 15 - 1				ம	တို့ တို့ တို့ တို့ တို့ တို့ တို့ တို့	
HETA-1 HETA-1 1.95 - 85 - 75 - 65554535251505 . 05 . 152535 HETA-1 1.00 0. 862 0. 863 0. 865 0. 865 0. 864 0. 877 0. 884 0. 874 0. 885 0. 895 0. 995			,			
HETALIVE EFFICIENCY OF GLS 10 QLS HETALIVE FFICIENCY OF GLS 10 QLS THETAL-1	,				5599777795670	
RELATIVE EFFICIENCY OF GLS TO						
HITM-1			-	``:	00+01+804616010	
RELATIVE EFFICIENCY OF GLS TO QLS THETA-2 HETA-1 100 0 865 0 855 - 75 - 65 - 55 - 45 - 35 - 25 - 15 - 05 05 15 2 HETA-1 100 0 865 0 885 0 885 0 885 0 885 0 885 0 889 0 899 0 890 0 89						
HETA-1						
RELATIVE EFFICIENCY OF GLS 10 DLS HETA-1 1.90		,			1 4 4 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6	
RELATIVE EFFICIENCY OF GLS 10 OLS HETA-1 1.90				D.	တစ်တို့ တို့ တို့ တို့ တို့ တို့ တို့ တို့	
HETA-1 1 90 0 852 1 91 0 925 - 85 - 75 - 65 - 55 - 45 - 35 - 15 - 15 - 05 0.05 1 90 0 852 1 90 0 852 1 90 0 852 1 90 0 852 1 90 0 853 1 90 0 853 1 90 0 854 1 90 0 854 1 90 0 855 1 90 0 8		.,	,	_	*	
HETA-1 1 90 0 852 1 91 0 925 - 85 - 75 - 65 - 55 - 45 - 35 - 15 - 15 - 05 0.05 1 90 0 852 1 90 0 852 1 90 0 852 1 90 0 852 1 90 0 853 1 90 0 853 1 90 0 854 1 90 0 854 1 90 0 855 1 90 0 8		ا بـ				
HETA-1 1 90 0 852		0			· · · · · · · · · · · · · · · · · · ·	
HETA-1 95857565554535251506 HETA-1 90 0.852				•	1 2 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	
HETA-1 HETA-2 HETA-2 HETA-1 HETA-2 HETA-2 HETA-2 HETA-2 HETA-2 HETA-3 HETA-1 HETA-2 HETA-3 HETA-1 HETA-2 HETA-2 HETA-3 HETA-3 HETA-2 HETA-2 HETA-3 HETA-2 HETA-2 HETA-3 HETA-2 HETA-2 HETA-3 _			LD.	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		
HETA-1 958575655545352515 HETA-1 90 0.852 0.864 0.865 0.864 0.865 0.867	٠ س	ட		, c		
HETA-1 1-95858575655545352515 HETA-1 190 0 882 0 884 0 887 0 889 0 889 0 889 0 889 0 889 0 889 0 889 0 889 0 889 0 889 0 889 0 889 0 889 0 889 0 889 0 899 0 902 0 0 889 0 890 0		0	2	'	1 .	
HETA-1 1 90	5	Š	TA-		*	
HETA-1 1 90	PEI	-	Ή		07077-8407-9-87-47-7006	
HETA-1 HETA-1 190	ΑÞ		-		80000000000000000000000000000000000000	
HETA-1 HETA-1 190		1			000000000000000000000000000000000000000	
HETA-1 1-96		ш		1		
HETA-1 1958575655545		<u> </u>				
HETA-1 190		⋖ !				
HETA-1 1.90 0.852 1.90 0.854 0.854 0.854 0.854 0.855 0.855 0.870 0.864 0.864 0.865 0.864 0.865 0.866 0.866 0.866 0.866 0.866 0.867 0.867 0.867 0.867 0.868 0.868 0.869 0.912 0.912 0.915 0.916 0.925 0.916 0.926 0.916 0.927 0.938 0.946 0.946 0.946 0.946 0.947 0.946 0.947 0.946 0.947 0.947 0.947 0.948 0.9	i	· · · · · ·		-		
HETA-1 1. 90 1. 95 1. 95 1. 95 1. 95 1. 95 1. 95 1. 95 1. 96 1. 96 1. 96 1. 97 1. 97 1. 97 1. 98 1					000000000000000000000000000000000000000	
HETA-1 1. 90				i	C & C & C & C & C & C & C & C & C & C &	
HETA-1 1.90				ro.		
HETA-1 1.90 0.852 1.50 0.864 0.864 0.864 0.864 0.864 0.864 0.864 0.864 0.864 0.864 0.864 0.864 0.864 0.864 0.864 0.864 0.864 0.865 0.864 0.865 0.867 0.867 0.869 0.869 0.907 0.9						
HE TA-1 1.90 0.852 1.40 0.846 0.848 0.848 0.848 0.848 0.848 0.848 0.848 0.848 0.853 0.863 0.863 0.863 0.863 0.863 0.863 0.863 0.863 0.863 0.863 0.863 0.863 0.863 0.863 0.863 0.863 0.863 0.863 0.904 0.905 0.907 0.907 0.908 0.907 0.908 0.908 0.909 0.				'		
HE TA-1 1.90 0.852 1.90 0.852 1.40 0.846 0.848 0.848 0.857 1.40 0.849 0.848 0.857 0.864 0.863 0.865 0.864 0.865 0.865 0.867 0.867 0.907 0.907 0.907 0.907 0.907 0.908 0.908 0.908 0.908 0.909 0.90					8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	
HETA-1 1.90 1.90 1.90 1.90 1.90 1.00						
HETA-1 1.90 1.90 1.90 1.90 1.90 1.00						
HETA-1 9585 1.90					88888890000000000000000000000000000000	
HE TA - 1 1. 90 1. 90 1. 90 1. 10 1. 10 1. 10 1. 10 1. 20 1. 20 1. 30 1. 20 1. 30 1. 20 1. 30 1. 20 1. 30 1. 20 1. 30 1. 30 1. 40 1. 20 1. 30 1. 40 1. 40 1. 40 1. 40 1. 50 1. 50 1. 50 1. 50 1. 50 1. 50 1. 63 1. 60 1. 60 1. 70 1. 10	,					
HE TA - 1 1. 90 1. 90 1. 90 1. 10 1. 10 1. 10 1. 10 1. 20 1. 20 1. 30 1. 20 1. 30 1. 20 1. 30 1. 20 1. 30 1. 20 1. 30 1. 30 1. 40 1. 20 1. 30 1. 40 1. 40 1. 40 1. 40 1. 50 1. 50 1. 50 1. 50 1. 50 1. 50 1. 63 1. 60 1. 60 1. 70 1. 10						
HE TA - 1 1. 90 1. 90 1. 90 1. 10 1. 10 1. 10 1. 10 1. 20 1. 20 1. 30 1. 20 1. 30 1. 20 1. 30 1. 20 1. 30 1. 20 1. 30 1. 30 1. 40 1. 20 1. 30 1. 40 1. 40 1. 40 1. 40 1. 50 1. 50 1. 50 1. 50 1. 50 1. 50 1. 63 1. 60 1. 60 1. 70 1. 10					4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	
HE TA - 1 1. 90						
H		,				
H					24448888888888888888888888888888888888	
HE TA - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	-			'		
# HE T T T T T T T T T T T T T T T T T T					1	
			ប		000000000000000000000000000000000000000	
				⊢	1	
			Ŀ	‡	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	

≱∳...

	1	
	95	· · · · · · · · · · · · · · · · · · ·
	"	17
1	85	000
	~	100 100 100 100 100 100 100 100 100 100
	<u>υ</u> ,	0000
	7.	T1000000
	5.2	00.000
	9	661 1332 001
	ιŭ	0000000
	ı.	88 776 660 660 67 73 88 82 73 86 73 86 74 74 74 74 74 74 74 76 76 76 76 76 76 76 76 76 76 76 76 76
	. ب	Ø 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	4	8 8 8 8 7 7 7 8 8 8 8 8 7 7 7 8 8 8 8 8
	C	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
	€.	74 n u l l m u u v o o o o o o o o o o o o o o o o o
	2	982 984 988 993 993 993 993 993 993 993 993 993
	2.	67 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
	. 2	մասասասասասագաւ-նու
S	- - -	υ + 4 π ω π υ α υ α υ α υ τ ν ν ο ο ω ζ ο ο ο ο ο ο ο ο ο ο ο ο ο ο ο ο ο ο ο
01.9	מ	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
- O I	Ö	- 470 0 4 0 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
2, '	2	961 962 963 974 974 989 989 989 989 989 989 989 989 989 98
ш ц	Ö	44 L O T D 4 D 4 D L D L D L D L D L D L D L D L
DIX CV O	٧ .	954 954 957 957 957 957 957 957 957 957 957 957
APPEND ICIENC	- I -	00000000000000000000000000000000000000
	1	946 946 946 946 966 966 966 967 97 97 97 97 97 97 97 97 97 97 97 97 97
E E E	. 25	0 0 0 4 + + 4 8 8 + + 1 8 + 4 4 4 1 1 1 + 1 0 0 + 4 + 1 0 + 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
VE		00000000000000000000000000000000000000
ATI	. 35	ω + ω ο ω ψ ω ν + 4 + ω ν 4 ω φ ο ω ο ο π ν ω π ω 4 4 ο ο ο ο ο ο ο ο ο ο ο ο ο ο ο ο ο
REL		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	45	
		928 930 930 930 930 930 930 930 930 930 930
	. 55	
	'	21 - 22 - 22 - 22 - 23 - 23 - 23 - 23 -
	.65	
	1	000000000000000000000000000000000000000
	75	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
	1	000000000000000000000000000000000000000
	85	00000000000000000000000000000000000000
-	1	00000000000000000000000000000000000000
	95	0 m 4 C 0 4 m 0 0 0 C 4 m C 0 0 m m m m 0 0 0 4 + C 0 0 0 7 0 C 10 C 10 0 0 7 C 10 0 0 0 7 C 10 0 0 0 0 7 C 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	,	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
	\	***************************************
•	A 1	980 100 100 100 100 100 100 100 1
	THET	
	· i -	

							*		99
	! .	· . I I	<i>t</i> :	I	-27	· 有形 :	, 9		
	· , `		95	-	. \$		0 4		
`		1			•		29 31 64	•	
			82		-, t		0.0 8.0 8.4	ī., ?	
	,		•			•	# 4 4 6 6 8 6 4 8 6 9 6 4 8 6		
	'.		75	>			8 C 0 C 0		
			•	j.,			8 3 6 3 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	`# 2	s of
			65			•	000000		•
		-					68 68 68 60 60 60 60 60 60 60 60 60 60 60 60 60		
			52	,		•		→ ************************************	**************************************
			•		,		882 721 731 805 805	- 4	T
			45		•	(υ <u>4</u>	u:
			•			0.0	8890 777 777 777 777 777	0 0 0	- N. T.
			35			ი.		o ro. 4	i
			•				0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		
ø		by 4	25			თ თ. ი		ன் ரெய் ம	4
	٠,		÷.	, j			0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	and the second s	
		£ 14	្ ក			တတ္တ			,
	S		•				9994 6 9994 6 9994 6 9998 6 9994 6 99		
	0	,	02	٠.					
	∃ £	-			ės,		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	· ·	
e.	GL		05	į.	12. - 12.1				
×	0	2	ï	Y-,,,		64 0 8 O 8 I	888 993 997 998	ល	ζ, φ.
=	ENCY	TĄ-:	ੇ ਹ	3 "	74	္တြက္တက္တက္က		9 9 9 8 7 6 9 9	
APPEND	CIE	THE	1	,	·	0-02-0	88888888888888888888888888888888888888	ထားထားကို က တႏထာ္ကစားထား 🗢 👡	
Ā	FFI		25		6.	တတ္တတ္တည့္		ი ი ი ი ი ⊢ ს ი −	,
	EE		 		55	75 10 10 10 10 10 10 10 10 10 10 10 10 10	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	887 880 80 80 80 80 80 80 80 80 80 80 80 80	
	ΥΙV		35				က က က က က က က က က က က		
	ELATI	35	i					8 7 7 9 8 2 8 8 5 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	\$;
	æ	14	45	,	ത്ത്	က္တက္တက္က	, , , , , , , , , , , , , , , , , , ,	00000000000	* .
			1	r		- D	•	8 7 8 7 8 7 5 7 7 7 7 7 8 7 8 7 8 7 8 7	ග
			55		95	96.	70 70 70 70 70 70 70 80	000 000 000 000 000 000 000 000 000 00	90.
			1	1.	ein.		g. ga	0000000000	O
			65	i.	មេខ១១១១១១១១១១១១១១១១១១១១១១១១១១១១១១១១១១១១	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	> □ <	9473 9973 9975 9975 9973 9973 9973 9973	185 046
			1					0000000000	
			2	<u>.</u>	ភព ភព ភព ភេស ភព ភព ភព ភព	9 9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	\$000000 \$00000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	30
3			. 7	,	· · · ·		· · · · · · · · ·		
4			2					<u>.</u>	
		1		948	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	95.00		963 963 957 957 937 937 937 758 758	9 43 43 43 43 43 43 43 43 43 43 43 43 43
٠. ،				000		000000	00000000		0000
×.	.s.'		. 95	3 4 6 8 4 8 4 8 8 4 8 8 8 8 8 8 8 8 8 8 8	552 151 159 159	955 956 954 953 950 960	961 953 957 953 953 953 953	905 905 905 905 905 905 905 905 905 905	525 160 122 152
:	, ·	-	'	1				9 9 9 9 9 9 9 9 9 7 7 7 9 9 9 9 9 9 9 9	A
		20							
		11	HETA	90 70	S 6 8 8			000000000000000000000000000000000000000	90.00
		ء` ا	∓	777	, , , , , ,	779999	00000000	000000	

					#LUU .
			1	94.6	
			95	0	
•			·	119 848 148	
			85	000	
			'	633 634 74 4 4 8	-
4		-	75	00000 8.0000	
				3 2 3 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	
			65	000000 000000 000000	•
•			- 1	3930.00 1730.00 1830.00 1830.00 1830.00	is.
			55	000000000000000000000000000000000000000	
,				88 88 9 7 2 2 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	
€.			45	000000000000000000000000000000000000000	
		4	. 4	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	•
			35		
	*	, es		00000000000000000000000000000000000000	
	ļ .	∂ p 13	25	000000000000000000000000000000000000000	
				000000000000000000000000000000000000000	
*			15		,
	S			8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	
	0 0		05		
	5 70		,	9889 9987 9987 9999 9999 9999 9999 9999	
4 ,	9.9		05		
ш ×	OF	5	, ,). '	6 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	
-	NC.Y	[A-2	5		
PEND	I E	LHE1	1	748 888 889 887 887 990 990 990 990 990 990 990 990 990 99	
AP	FIC		ស ·		
, make	in in		\cdots 	2 9 7 8 9 7 7 8 9 8 9 7 7 8 8 9 7 7 8 9	
	7106	τ.	35		
•	£LA]		ı	272 272 272 272 272 288 288 288 288 288	
	à		5		
			4,		
			35	00000000000000000000000000000000000000	
		ţ.	5		-
			. 29	666 666 667 667 677 677 677 677 677 677	
4			9		
		*	_	ត់តំប៉ុន្ឌិល១០+ប្រុងពិប្រុក្សិន នេះ នេះ ១០១១១១១១១១១១១១១១១១១១១១១១១១១១១១១១១១១១១	
	٥		. 75	996669999999999999999999999999999999999	
f			l		
			85	90000000000000000000000000000000000000	025
			'		•
			95	662 662 664 666 666 666 667 667 667 668 668 668 668	20
			1		- 0
		30	+		
		11	Δ T	088 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	90
		c	7HE		

Ŋ.	
ú	
NDIX	
bbEl	
4	

OLS
10
GLS
0F
EFFICIENCY
RELATIVE

 				<u>-</u>								101
1	95		<i>i</i> .	, 9 <u>.</u>		. *		0 7 6	7	¥ .		· ·
	35		: -	, AGL			**		2.			
	, 80				S			879 803 0	62 8			- ·
a	. 75			er F				900				-,
	. 65						o C		0.69 0.47 0.24	à		
	55						סַס	ითი	0.844 0.844 0.717 0.495	7		,
						-	93	284	(t)	00 1 1	<i>;</i>	
	.45	Ĺ					95 96 0. 96 0.	0 00 0	2 4 4 4	0.00	į	
!	. 35							, 0, 0, 0	၈၈၈	7 2		
	25				۸.	66	6 6 6 6 7	66.	. 98 . 98 . 94	0.884 0.763 0.525	7.7.	
						94 95	96	0000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	947 890 769	50	
	15									976 0. 949 0. 892 0.		
	.05				,	000	0000	0	-000	0000	000	•
	05					0.991 0.992 0.992 0.993						
1-2	ا ا		•		88	90 94 92	000 004 001	96	0000	94	9882 8882 752 490 146	
THETA	<u>.</u>	}			10 ~ 0	ം തെ ത	- 20 00 5	1000	- m m -	10 m i	935 935 870 734 966 965)
	. 25				000		000	000	000		00000)
	35		* *	·	8 8 8 8		စ္ ၈ ၈ ၈ ၈ ၈ ၈ ၈	66.		96	0.977 0.959 0.924 0.854 0.711	
	Ω.	:		တ	ω	σασα	യയതൗ	nono	nooo	တတထဖ	949 949 910 834	0 00
	4.			~ 2	004	1 ហ ហ ហ (- L 8 0	000+		- 6 ~ 0	an - y a o o o o o o	~ U D c
	55			თ თ	0000	0,000	<u>ი</u> ი ი ი	၈ တ တ	၈ တ တ တ	တတ္တ	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	, φ, φ, Q,
	. 65	,		86.8	86.	86.0	8 8 8 8	96.6	86. 86. 86.	86	982 976 956 950 923	34.05
	5		. 62	000	0 '0	, a a a .	4 4 V R	വരം	் மம்	യമാന	80 0 69 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	80 - 030
	T		<u>ი</u>	თთი	დიი	၈ တ တ တ	ი ი ი ი	n o o o	, o o o	တ္တက္	3 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	0 0 0 0 0
	85	,	97	97	86.	0 0 0 0	866	866	0 0 0 0 0 0 0 0 0 0 0	8 8 6	96.	889 9 828 9 723 545 0 280 0 040
	95		77 77 77	77 78 79	79 79	880	887 824 824	2000	8 8 3 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	81 80 79	7 7 8 9 7 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9	8804 8804 6890 6690 5099 0333
09	-	1										0000000
S = ù	THE TA-				-1.30						0000	90 90 90 90 90 90
											_	

	1		í	8
			95	•
	,		2	745. 515. 185
ŗ.			, <u>e</u>	90 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
			75	6 & F & F
			_	977 9939 939 196 196
		,	. 65	00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
•			55	00.000 00.000 00.000 00.000 00.000 00.000
		-		996 9996 9997 9976 9976 9976
			. 45	α α α ν ο 4 υ ο υ υ υ ω 4 ο ο ο ο ο ο ο ο ο ο ο ο ο ο ο ο ο ο ο
			35	
	,			00000000000000000000000000000000000000
			. 25	00000000000
			2	9997 9999 9999 9999 9997 9977 9997 999
	r S		- .	9996 9996 9997 9999 9999 9999 9999 9999
	10 0		. 05	00000000000000
9	GLS		Б	00000000000000000000000000000000000000
ш	OF	2	0.	
END I	ENCY	T A -	<u> </u>	őőőőőőőőőőőőőőőőőőőőőőőőőőőőőőőőőőőőő
АРР	101	THE	1	99999999999999999999999999999999999999
	ÉFF	,	- 25	00000000000000000000000000000000000000
_	TIVE		35	00000000000000000000000000000000000000
	RELA		, 1	00000000000000000000000000000000000000
			. 45	
		-	55	00000000000000000000000000000000000000
			1	000++++44444444444460+868008048P
			65	
			- 75	
			85	88888888888888888888888888888888888888
			1	
	,		- 95	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
		00		000000000000000000000000000000000000000
		10	A T	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
		С	THE	

			·		103
	1	Ţ		016	,
			95		
J				020 025 066	
			85		
			,	, , 015 980 991 026	96
		}	75		•
			·	55 7.39 7.39 9.99	940
			65	- O O O O	0,0
	,		•	008 002 66 66 84	
		i	55		
				777 335 883 668 672	0400
			45		and the second s
				253 0072 001 979 979	8 8 O 4 O
			35	0000 0000	
			·	3339 112 018 988 989 989	81 75 75 89 93 03 03
			25		
				134 134 136 136 136 136 136 136 136 136 136 136	8 Q U 4 Q O Q
			1 5		· · · · · · · · · · · · · · · · · · ·
	01.5			2000 6003 6000 6000 6000 6000 6000	86 669 772 83 772 83
	T0		05		
	YPX			6661 294 102 102 103 103 103 103 103 103 103 103 103 103	080 075 075 075 075 075 075 075 075 075 07
н. -	F MA		. 05		
	0	-2	· '	791 158 158 158 000 000 991 992 992	100 110 110 110 110 110 110 110 110
APPENDIX	:NC Y	TA-	15		
APP	FICIENC	THE	1	928 506 0037 0029 903 907 907 907 907 909	200 200 200 200 200 200 200 200 200 200
	EFF		25		00000000
	VE 1		,	068 344 175 175 175 175 176 177 177 177 177 177 177 177 177 177	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	ATI		35		0000000000
	REL		'	205 799 799 172 172 100 005 100 005 999 969 969 969 969	99999999999999999999999999999999999999
	_		.45	N0000000	
			'	332 9649 6649 303 201 211 211 200 90 90 90 90 90 90 90 90 90 90 90 90 9	003 9988 9989 9980 7598 7598 7598 774 774 774 774 774 774 774
			. 55	N = = = = = = = 00000000	
			I	, 130 130 617, 479, 377 138 0054 0054 0005 0005	23 24 25 26 27 27 27 27 27 27
			. 65		
			:	4 10 E = E 3 = 10 F E 2 10 E E E E E E E	10 × = 10 10 0 × 00 0 (0 10 0 × 0 0 0 0
			75	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	000 000 000 000 000 000 000 000
-			,	000	000000000
	i		85	625 625 625 625 625 625 749 749 749 162 162 162 163 163 163 163 163 163 163 163 163 163	142 127 107 107 107 107 107 107 107 107 107 10
				and the control of th	
			95	1	0.1 C C C C C C C C C C C C C C C C C C C
			0,	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	000000-0440-0000
		`	<u> </u>	2222221	
		: 5	- W	000 000 000 000 000 000 000 000 000 00	
		יי	HET	00000000000	the contract of the contract o
1			· -		

L	_	
;	×	
۱	-	
ĺ	₹	
•	Z	
ι	u	
	1	
	7	
•	٩	

RELATIVE FFFICIENCY OF MADYX T THE LATIVE FFFICIENCY OF MADYX T THE LATE THE LATIVE FFFICIENCY OF MADYX T THE LATE THE L	THE LATIVE ET FICTION OF MADY 10 OLS THE LATIVE FOR THE LATIVE FO	PS - 75							,												
THE LA-2 5 775 - 65 - 55 - 65 - 65 - 65 - 75 - 75	THE LA-2 5 - 75 - 65 - 55 - 45 - 35 - 25 - 15 - 05 05 15 25 - 35 45 55 65 75 60 2 4 767 60 3 10 1 4 478 60 2 5 14 4 478 60 2 10 1 1 10 1 10 10 10 10 10 1 10 1 1	THE LA. 2 5 75	ļ	on a management	THE CHAPTER OF THE MALLOCAL COMPA			ATI	VE EFF	ICIENC	Y 0F M	σ .	J								
5 775 - 65 - 55 - 45 - 35 - 25 - 15 - 15 - 15 - 15 - 15 - 15 - 1	55 - 755 - 655 - 556 - 455 - 35 - 125 - 11505	5 - 75	ĺ							-	2										
95 4 767 4 478 95 5 1413 2 240 4 147 96 1 2 1413 2 240 4 147 97 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9.6 3 5511 4.478 9.7 571 4.478 9.8 1 5511 4.478 9.8 2 5511 4.8 2 511 4.	2 4 767 4 478 5 14 4 478 6 1369 3 781 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		2	5	. 65	. 5	£	. 2		0.										
99 9 1767 478 91 1 4 478 92 1 1 4 478 93 1 1 4 478 94 1 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	96 1 767 4 767 4 768 6 3 781 6 3 781 6 3 781 6 3 781 6 3 781 6 3 781 6 3 781 6 3 781 6 3 781 6 3 781 6 3 781 6 3 781 6 3 781 7	98						-													
95 5 4 75 7 4 478 95 2 4 75 7 4 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8	06	06 2 1415 2 3040 4 117 8 118 1 257 1 397 8 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1					•			-							,				
96 3 17 4 478 97 3 17 4 478 98 3 5 17 4 478 98 3 5 17 4 478 98 3 5 17 4 478 98 3 5 17 4 478 98 3 5 17 4 478 98 3 5 17 4 478 99 3 5 17 4 478 99 3 5 17 4 478 90 3 17 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1	8. 3 5 11 4 478 8. 5 2 875 3 0.40 8. 6 2 877 5 1 0.41 8. 6 2 877 5 1 0.41 8. 6 2 877 5 1 0.41 8. 6 2 877 5 1 0.41 8. 6 2 877 5 1 0.41 8. 6 2 877 5 1 0.41 8. 6 2 877 5 1 0.41 8. 6 2 877 5 1 0.41 8. 6 2 877 5 1 0.41 8. 6 2 877 5 1 0.41 8. 6 2 877 5 1 0.41 8. 6 2 877 6	9. 3. 767 9. 10. 1 9. 1 9. 10. 1 9.		(€ ⁷¹										
56 2.875 3 040 0 1417 1418 1 25 0.608 3 784 1 1417 1418 1 25 0.608 1 1417 1418 1 25 0.608 1 1417 1418 1 25 0.608 1 1417 1418 1 25 0.608 1 1417 1418 1 25 0.608 1 1417 1418 1 25 0.608 1 1417 1418 1 25 0.608 1 1417 1418 1 1417 1418 1 25 0.608 1 1417 1417	56 2 417 3 040 4 1478 56 2 417 3 040 4 1478 56 2 417 3 040 4 1478 56 2 417 3 040 4 1478 56 2 417 3 040 4 1478 56 2 417 3 040 4 1478 56 2 417 3 1991 1 9918 2 1237 3 1997 57 1 574 1 468 1 567 1 614 1 9930 3 0099 78 1 574 1 468 1 567 1 614 1 9930 3 0099 79 1 440 1 252 1 1451 1 188 1 1255 1 4921 2 288 79 1 440 1 252 1 1451 1 188 1 1255 1 4921 2 288 79 1 440 1 252 1 1451 1 188 1 1255 1 4921 2 288 79 1 440 1 252 1 1481 1 188 1 1255 1 4921 2 288 79 1 440 1 252 1 1481 1 188 1 1255 1 4921 2 288 79 1 440 1 252 1 1481 1 188 1 1255 1 4921 2 288 79 1 440 1 252 1 1481 1 148 1 1255 1 4921 2 288 79 1 440 1 252 1 1481 1 1481 1 1251 1 1481 1 1481 1 1251 1 1481	28 3 5 11 4 478 55 2 875 3 0.40 4 147 56 2 875 3 0.40 4 147 51 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		9 &	76		٠														
\$\frac{5}{2}\$ 2 475 5 0.00 \text{ 4 147} \$\frac{7}{2}\$ 1 0.00 \text{ 4 147} \$\frac{7}{2}\$ 1 0.00 \text{ 4 147} \$\frac{7}{2}\$ 2 6.00 \text{ 3 176} \$\frac{7}{2}\$ 1 0.00 \text{ 4 147} \$\frac{7}{2}\$ 1 0.00 \text{ 4 147} \$\frac{7}{2}\$ 1 0.00 \text{ 4 157} \$\frac{7}{	5.5 2.875 5.00 4.0 4.147 6.00 4.147 6.00 4.147 6.00 4.147 6.00 4.10 4.147 6.00 4.147 6.00 4.147 6.00 4.147 6.00 4.147 6.00 4.1252 6.00 6.00 6.00 6.00 6.00 6.00 6.00 6.0	2. 8 75 2 100 4 147 1 100 1 10		× 6	111														No.		
512 1 468 1 517 2 518 2 518 2 518 1 518 1 518 1 518 1 518 1 518 2	7.6 2 1413 2 335 2 608 3 781. 2.1 2 1 648 1 55.7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1,000 1,00	. ~	56	875		14											•	· 'r	_	
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	1.0 1.0	212 1 1868 1 151 1 1918 2 127 3 397 3 009 213 1 1868 1 1567 1 1614 1 1930 3 009 214 1 1868 1 1567 1 1614 1 1930 3 009 215 1 161 1 1684 1 1930 3 1 400 1 1684 2 1635 217 1 161 1 168 1 168 1 169 1 168 1		65	413		608	8											- '(.		
112 1 668 1 648 1 567 1 614 1 303 3 0.09 11521 1 668 1 648 1 567 1 614 1 303 3 0.09 11521 1 668 1 648 1 567 1 614 1 303 3 0.00 11521 1 671 1 688 1 1567 1 1303 1 1.00 11521 1 617 1 618 1 1.00 11521 1 617 1 618 1 1.05 11521 1 617 1 618 1 1.05 11521 1 617 1 618 1 1.05 11521 1 617 1 618 1 1.05 11521 1 617 1 618 1 1.00 11521 1 617 1 618 1 1.05 11521 1 617 1 618 1 1.05 11521 1 617 1 618 1 1.05 11521 1 617 1 618 1 1.05 11521 1 617 1 618 1 1.05 11521 1 617 1 618 1 1.05 11521 1 617 1 618 1 1.05 11521 1 617 1 618 1 1.05 11521 1 617 1 618 1 1.05 11521 1 617 1 1.05 11521 1 617 1 618 1 1.05 11521 1 617 1 618 1 1.05 11521 1 617 1 618 1 1.05 11521 1 617 1 618 1 1.05 11521 1 617 1 1.05 11	912 1 666 1 648 1 562 1 614 1 930 3 009 914 1 614 1 930 3 009 915 1 671 1 468 1 360 1 1684 1 532 0 809 915 1 671 1 468 1 360 1 1360 1 1684 1 535 1 1401 1 684 2 2.889 917 1 671 1 468 1 360 1 1360 1 1684 1 255 1 1492 2 2.889 918 1 610 1 605 1	212 1 666 1 648 1 567 1 614 1 390 3 009 397 1 657 1 468 1 360 1 333 1 401 1 684 2 535 3987 1 657 1 468 1 360 1 333 1 401 1 684 2 535 3997 1 657 1 468 1 360 1 333 1 401 1 684 2 535 3997 1 657 1 468 1 360 1 333 1 401 1 684 2 535 3997 1 657 1 468 1 360 1 333 1 401 1 684 2 535 3998 1 534 3 40 1 225 1 497 1 408 1 40		5	108		918	37 3.	ത												
997 1671 1468 1360 1333 1401 1684 2.539 9173 1534 130 1535 1187 1188 11255 1432 2.289 9173 1534 130 1525 1187 1188 11255 1432 2.289 9173 1534 130 1525 1187 1188 11.055 1037 1030 1158 1348 1982 9174 140 1 252 1154 1055 1037 1030 1155 1031 1048 1327 9175 1242 1162 1052 1053 1035 1030 1158 1348 1982 9175 1242 1162 1031 1005 1038 0.995 0.	937 1.671 1.468 1.356 1.333 1.401 1.684 2.635 873 1.534 1.340 1.255 1.197 1.188 1.255 1.255 1.395 873 1.534 1.340 1.255 1.197 1.188 1.255 1.435 1.381 873 1.534 1.340 1.255 1.197 1.188 1.255 1.435 1.381 874 1.440 1.252 1.154 1.005 1.005 1.007 1.005 1.006 1.006 1.005 1.007 875 1.340 1.411 1.006 1.005 1.007 1.003 1.006 1.006 1.007 1.003 1.006 1.007 875 1.242 1.105 1.003 1.008 0.992 0.997 0.995 1.007 1.003 1.004 1.005 1.007 875 1.242 1.105 1.001 0.988 0.991 0.995 0.997 0.995 0.997 0.99	997 1.671 1.468 1.360 1.333 1.401 1.684 2.635 773 1.340 1.252 1.187 1.188 1.255 1.492 2.289 774 1.440 1.252 1.187 1.188 1.255 1.492 2.289 775 1.440 1.252 1.187 1.188 1.255 1.492 2.289 776 1.340 1.252 1.187 1.188 1.255 1.492 2.289 777 1.440 1.252 1.187 1.188 1.255 1.492 2.289 778 1.340 1.252 1.187 1.087 1.005 1.005 1.005 1.005 1.007 1.004 1.016 1.505 779 1.240 1.141 1.063 1.005 1.005 1.005 1.005 1.007 1.004 1.010 1.018 1.0059 1.187 771 1.206 1.080 1.025 0.991 0.981 0.981 0.981 0.991 0.991 0.991 0.991 0.991 0.991 0.991 778 1.176 1.001 1.001 0.984 0.981 0.981 0.981 0.991 0.991 0.991 0.991 0.991 0.991 0.991 779 1.176 1.001 0.984 0.981 0.981 0.981 0.991 0.991 0.991 0.991 0.991 0.991 0.991 0.991 770 1.007 1.010 0.984 0.981 0.981 0.991		12	868		562	14 1	30	_ 0									э		
873 1.534 1.340 1.235 1.187 1.188 1.255 1.289 1.492 2.289 1.400 1.205 1.105 1.087 1.081 1.081 1.981 1.982 1.481 1.982 1.481 1.982 1.481 1.982 1.481 1.982 1.481 1.982 1.481 1.982 1.481 1.982 1.481 1.982 1.482 1.	773 1.534 1.340 1.235 1.187 1.188 1.255 1.482 2.289 774 1.440 1.525 1.154 1.009 1.188 1.255 1.482 2.289 775 1.440 1.526 1.154 1.009 1.188 1.255 1.481 1.881 776 1.340 1.340 1.252 1.154 1.009 1.188 1.355 1.481 1.881 777 1.440 1.327 1.481 1.005 1.005 1.003 1.005 1.005 1.007 1.004 1.005 778 1.340 1.340 1.055 1.007 1.005 1.005 1.005 1.007 1.004 1.005 775 1.440 1.006 1.005 1.005 1.007 1.005 1.007 1.004 1.004 1.005 775 1.440 1.006 1.005 1.007 1.005 1.007 1.005 1.007 1.004 1.007 1.007 777 1.206 1.006 1.002 0.991 0.991 0.991 0.991 0.991 0.991 0.991 0.991 0.991 0.991 0.991 778 1.406 1.007 0.991	1.534 1.340 1.235 1.487 1.188 1.255 1.482 2.289 1.484 1.982 1.484 1.982 1.484 1.985 1.484 1.985 1.484 1.985 1.484 1.985 1.484 1.985 1.484 1.985 1.484 1.985 1.484 1.985 1.484 1.985 1.484 1.985 1.484 1.985 1.484 1.985 1.484 1.985 1.484 1.985 1.484 1.985 1.484 1.985 1.484 1.985 1.484 1.985 1.985 1.984 1.985 1.98	-	7.0	671		360	33	, -	c	ď								r ⁱ		
779 1.400 1.252 1.152 1.105 1.087 1.089 1.188 1.982 1.188 1.982 1.189 1.	779 1 440 1 252 1 152 1 105 1 108 1	779 1.440 1.252 1.152 1.105 1.087 1.089 1.188 1.088 1.088 1.081		. 6	ָ ער	340	2000	+87 1	- a	· -	000	a							•		
678 1.362 1.189 1.100 1.055 1.035 1.038 1.048 1.096 1.240 1.759 582 1.189 1.100 1.055 1.001 1.005 1.000 1.005 1.000 1.057 1.162 1.502 583 1.294 1.141 1.1005 1.005 1.000 1.000 1.005 1.000	678 1.362 1.189 1.100 1.055 1.035 1.031 1.048 1.066 1.240 1.79 582 1.224 1.141 1.062 1.025 1.003 1.002 1.005 1.033 1.048 1.066 1.240 1.104 512 1.244 1.141 1.062 1.025 1.005 1.003 1.005	542 1.156 1.169 1.100 1.055 1.035 1.038 1.048 1.036 1.240 1.715 542 1.124 1.141 1.063 1.025 1.035 1.035 1.035 1.048 1.036 1.240 1.715 542 1.105 1.063 1.025 1.037 1.025 1.035 1.035 1.034 1.104 1.327 442 1.105 1.036 1.005 1.005 1.036 0.984 0.985 0.985 1.007 1.018 1.059 1.187 442 1.105 1.036 1.005 0.984 0.985 0.987 0.983 0.995 1.001 1.018 1.059 1.007 443 1.106 1.036 1.036 0.984 0.985 0.987 0.995 0.995 0.997 0.995 0.997 0.095 0.997 0.995 444 1.001 0.984 0.982 0.981 0.980 0.995 0.995 0.997 0.997 0.995 0.997 0.995 0.997 0.995 0.997 0.995 0.997 0.995 0.997 0.995 0.997 0.995 0.997 0.997 0.995 0.997 0.995 0.997 0.995 0.997 0.997 0.995 0.997 0.995 0.997 0.995 0.997 0.995 0.997 0.		279	. 4		15.4	107	. +		32 Z.	48 4 0	α				4			_	
582 1, 294 1, 141 1, 1063 1, 1025 1, 1007 1, 1002 1, 1007 1, 1002 1, 1007 1, 1002 1, 1007 1, 1002 1, 1007 1, 1002 1, 1007 1, 1002 1, 1007 1, 1002 1, 1	582 1 294 1 1141 1 1006 0 392 0 397 1 029 1 1007 1 1009 1	542 1 294 1 141 1 1063 1 1025 1 1007 1 1005 1 1007 1 1005 1 1007 1 1018 1 1025 1 1007 1 1018 1 1025 1 1007 1 1018 1 1025 1 1007 1 1018 1 1005 1 1007 1 1018 1 1005 1 1007 1 1018 1 1005 1 1007 1 1018 1 1005 1 1007 1 1018 1 1005 1 1007 1 1018 1 1005 1 1007 1 1018 1 1005 1 1007 1 1018 1 1005 1 1007 1 1018 1 1005 1 1007 1 1018 1 1005 1 1007 1 1018 1 1005 1 1007 1 1018 1 1005 1 1007 1 1018 1 1005 1 1007 1 1018 1 1005 1 1007 1 1018 1 1005 1 1007 1 1018 1 1005 1 1007 1 1018 1 1005 1 1007 1 1018 1 1005 1 1007 1 1018 1 1007		678,	96				. ב		. •	0 90	7 0	4 +							
5.15 1.242 1.105 1.005 1.005 0.992 0.997 0.993 0.995 1.007 1.001 1.004 1.327 4.71 1.206 1.005 1.002 0.995 0.997 0.993 0.993 1.001 1.001 1.001 0.994 0.993 1.002 1.001 1.001 0.994 0.993 0.993 0.994 0.993 0.994 0.995 0.993 0.995 0.993 0.995 0.993 0.995 0.993 0.995 0.995 0.993 0.995	515 1.242 1.105 1.038 1.006 0.992 0.987 0.985 1.001 1.031 1.002 0.995 0.984 0.995 1.001 1.001 1.001 1.001 1.001 0.995 0.984 0.995 0.984 0.987 0.995 0.984 0.987 0.995 0.984 0.987 0.995 0.996 0.995 0.996 0.995 0.994 0.997 0.997 0.997 0.997 0.997 0.996 0.999 0.997 0.997 0.999 0.997 0.999 0.997 0.997 0.997 0.999 0.999 0.997 0.999 0	5.15 1.242 1.105 1.008 1.006 0.992 0.997 0.989 0.995 1.007 1.034 1.104 1.327 4.71 1.206 1.080 1.022 0.995 0.984 0.982 0.997 0.993 0.995 1.007 1.034 1.107 1.002 4.71 1.206 1.080 1.022 0.995 0.984 0.982 0.987 0.993 0.995 0.994 0.995 0.997 0.997 0.997 0.997 0.997 0.997 0.997 0.998 0.997 0.998 0.997 0.998 0.997 0.998 0.997 0.998 0.997 0.997 0.998 0.997 0.998 0.997 0.997 0.998 0.997 0.998 0.997 0.998 0.997 0.998 0.997 0.998 0.997 0.998 0.997 0.998 0.997 0.998 0.997 0.998 0.997 0.997 0.998 0.998 0.998 0.997 0.998 0.997 0.998 0.998 0.998 0.997 0.997 0.998 0.998 0.998 0.998 0.997 0.997 0.998 0.998 0.998 0.998 0.997 0.997 0.998 0.999		582	294		063	025 1	. 1	· -	. +	30 T OC	. t	-3 62 1	60				-		
471 1.206 1.080 1.022 0.995 0.984 0.982 0.987 0.987 1.001 1.018 1.059 1.87 1.87 1.206 1.080 1.022 0.995 0.995 0.997 0.998 0.999 0.99	471 1.206 1.080 1.022 0.995 0.984 0.982 0.987 0.997 1.001 1.018 1.059 1.87 425 1.776 1.020 1.0010 0.988 0.981 0.981 0.987 0.997 1.001 1.018 1.059 1.87 426 1.776 1.001 0.984 0.981 0.981 0.981 0.991 0.992 0.993 0.995	471 1.206 1.080 1.022 0.995 0.984 0.982 0.987 0.997 1.001 1.018 1.052 1.187 4825 1.176 1.020 1.080 1.022 0.995 0.984 0.982 0.983 0.987 0.991 0.994 0.997 1.002 1.017 0.017 388 1.176 1.061 1.001 0.988 0.984 0.982 0.983 0.987 0.995 0.9		515	. 242		038 1	000	92 0	C	- C	5		34 1 1	-	Loc					
425 1.176 1.061 1.0010 0.988 0.981 0.980 0.983 0.987 0.997 1.002 1.0077 1.072 1.017 1.072 1.017 1.072 1.017 1.072 1.017 1.002 1.017 1.002 1.017 1.002 1.017 1.002 1.0017 1.0017 1.0010 0.988 0.981 0.986 0.981 0.995 0.9	425 1.176 1.061 1.010 0.988 0.981 0.980 0.983 0.987 0.991 0.995 0.995 1.007 1.072 0.984 0.985 0.985 0.995 0.	425 1.176 1.061 1.010 0.988 0.981 0.980 0.983 0.987 0.991 0.995 0.997 1.002 1.017 1.072 368 1.146 1.004 1.0010 0.988 0.981 0.980 0.983 0.987 0.995 0.995 0.995 0.975 0.976 0.976 368 1.146 1.004 0.984 0.981 0.980 0.982 0.980 0.995 0.9		471	. 206	•	.022	95 0.	84 0.	Ö	83 0.	87 0.	. —			, ה ה	α				
368 1.146 1.044 1.001 0.984 0.986 0.986 0.996 0.995 0.995 0.995 0.997 0.972 0.976 0.907 0.907 0.907 0.908 0.909 0.997 0.998 0.997 0.997 0.998 0.997 0.998 0.997 0.998 0.997 0.998 0.997 0.998 0.997 0.998 0.997 0.998 0.997 0.998 0.999 0.998 0.998 0.999 0.	368 1.146 1.004 1.001 0.984 0.986 0.986 0.993 0.993 0.993 0.993 0.995 0.903 0.908 0.903 0.903 0.909 0.993 0.995 0.903 0.908 0.999 0.	368 1.146 1.004 1.001 0.984 0.982 0.986 0.995 0.993 0.995 0.995 0.997 0.919 0.		425	. 176	•	010	88 0.	810.	0	83 0.	87 0.	C	· c	0 1 26	. +	17 1	. 61			
144 1.19 1.030 0.994 0.982 0.981 0.984 0.989 0.997 0.9	144 1.119 1.030 0.994 0.982 0.981 0.984 0.989 0.997 0.996 0.997 0.996 0.997 0.996 0.997 0.996 0.997 0.996 0.997 0.996 0.997 0.996 0.997 0.996 0.997 0.996 0.997 0.996 0.997 0.996 0.997 0.996 0.997 0.996 0.996 0.997 0.996 0.	144 1.119 1.030 0.994 0.981 0.981 0.984 0.989 0.994 0.997 0.996 0.997 0.996 0.997 0.996 0.997 0.997 0.998 0.997 0.998 0.997 0.996 0.998 0.997 0.998 0.997 0.998 0.997 0.998 0.997 0.998 0.999 0.		368	. 146		00	84 0.	80 0.	0	86.0	90 06	c	0 56		. 0	. c	0	Ų.		
277 1.097 1.017 0.988 0.981 0.982 0.987 0.993 0.997 0.999 0.997 0.988 0.972 0.950 0.922 0.885 0.904 254 1.081 1.009 0.984 0.980 0.984 0.990 0.996 0.999 0.997 0.999 0.997 0.995 0.997 0.995 0.997 0.995 0.997 0.995 0.997 0.995 0.997 0.995 0.997 0.995 0.995 0.997 0.995 0.99	277	277 1 097 1 017 0 988 0 981 0 982 0 987 0 993 0 997 0 998 0 997 0 998 0 997 0 998 0 997 0 998 0 997 0 998 0 997 0 998 0 997 0 998 0		314	119		.994 0	82 0.	810.	0	89 O.	94 0.	0	0 96	0 -	2 6	. 6	90	0	-	
254 1.081 1.009 0.984 0.980 0.984 0.996 0.996 0.999 0.999 0.999 0.997 0.997 0.907 0.985 0.997 0.907 0.987 0.907 0.987 0.907 0.987 0.997 0.997 0.997 0.999 0.	254 1.081 1.009 0.984 0.980 0.984 0.996 0.996 0.999 0.	254 1.081 1.009 0.984 0.980 0.984 0.990 0.996 0.999 0.999 0.999 0.997 0.980 0.902 0.982 0.992 0.995 0.		277	.097		988 0	810.	82 0.	ò	93 0.	97 0	0	0 26	ο σ ο σ) C	0 0		
1068 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	136 1.068 1.003 0.983 0.981 0.985 0.992 0.997 0.999 0.996 0.985 0.965 0.937 0.907 0.885 0.894 0.953 1.058 0.999 0.982 0.981 0.985 0.995 0.999 0.986 0.996 0.996 0.996 0.996 0.996 0.996 0.996 0.997 0.998 0.999 0.998 0.999 0.998 0.999 0.998 0.999 0.998 0.999 0.998 0.998 0.999 0.998 0.999 0.998 0.999 0.998 0.999 0.996 0.999 0.996 0.999 0.996 0.999 0.996 0.999 0.996 0.999 0.996 0.999 0.996 0.999 0.996 0.999 0.996 0.999 0.996 0.999 0.996 0.999 0.996 0.999 0.996 0.999 0.996 0.999 0.996 0.999 0.996 0.999 0.999 0.996 0.999 0.	168 1.068 1.003 0.983 0.981 0.985 0.992 0.997 0.999 0.996 0.985 0.997 0.997 0.997 0.997 0.997 0.997 0.997 0.997 0.997 0.997 0.998 0.985 0.997 0.997 0.998 0.988 0.998 0.998 0.998 0.998 0.998 0.998 0.998 0.998 0.998 0.998 0.998 0.998 0.998 0.998 0.998 0.998 0.999 0.999 0.999 0.999 0.999 0.999 0.999 0.999 0.999 0.999 0.997 0.996 0.998 0.997 0.996 0.997 0.996 0.997 0.997 0.996 0.997 0.996 0.997 0.997 0.997 0.997 0.996 0.997 0.997 0.997 0.997 0.997 0.997 0.997 0.997 0.997 0.997 0.997 0.998 0.997 0.997 0.997 0.997 0.997 0.998 0.999 0.997 0.997 0.996 0.997 0.996 0.999 0.		254	.081		.984 0	80 0.	84 0.	0	96 0.	.0 66	0	94 0	0.0	59 0.			, C	, F	-
115 1 (1) 558 (1) 999 (1) 998 (1) 998 (1) 999	155 1 (1) (1) (1) (1) (1) (1) (1) (1) (1) (215 1 058 0 0999 0 0982 0 0981 0 0986 0 0991 0 0986 0 0986 0 0986 0 0940 0 0986 0 0988 0 0946 0 0946 0 0948 0 0988 0 0946 0 0989 0 0989 0 0989 0 0989 0 0989 0 0975 0 0976 0 0978 0 0978 0 0978 0 0978 0 0978 0 0978 0 0978 0 0978 0 0978 0 0979 0 0989 0 0976 0 0979 0 0989 0 0976 0 0979 0 0989 0 0976 0 0979 0 0989 0 0976 0 0979 0 0979 0 0979 0 0979 0 0979 0 0979 0 0979 0 0979 0 0979 0 0970 0 0989 0 0970 0 0989 0 0979 0 0979 0 0979 0 0979 0 0979 0 0979 0 0979 0 0979 0 0979 0 0979 0 0970 0 0989 0 0970 0 0979 0 0979 0 0979 0 0970 0 0979 0 0979 0 0979 0 0979 0 0970		236	.068	•	.983 0	810.	85 0.	0	97 0.	99 0.	0	85 0.	50.0	37 0.	07 0) C	20.0		•
189 1 047 0 996 0 980 0 979 0 983 0 987 0 988 0 982 0 966 0 940 0 906 0 878 0 936 1 668 100 1 035 0 989 0 975 0 974 0 976 0 978 0 973 0 959 0 933 0 898 0 866 0 863 0 921 1 063 134 1 019 0 997	189 1.047 0.996 0.980 0.979 0.983 0.987 0.988 0.986 0.940 0.906 0.878 0.878 0.936 1.868 160 1.035 0.989 0.975 0.974 0.976 0.978 0.973 0.959 0.933 0.898 0.866 0.878 0.921 1.063 1.34 1.019 0.976 0.976 0.976 0.978 0.979 0.933 0.898 0.866 0.867 0.921 1.063 1.010 0.997 0.997 0.996 0.996 0.996 0.996 0.996 0.996 0.996 0.997 0.997 0.997 0.997 0.997 0.997 0.997 0.997 0.997 0.997 0.997 0.998 0.875 0.898 0.875 0.897 1.024 1.024 1.024 1.024 1.034 1.003	189 1.047 0.996 0.980 0.979 0.983 0.987 0.988 0.982 0.966 0.940 0.906 0.878 0.878 0.936 1.067 1.035 0.989 0.975 0.974 0.976 0.978 0.973 0.989 0.933 0.898 0.975 0.974 0.976 0.978 0.973 0.989 0.936 0.937 0.921 1.063 1.34 1.019 0.976 0.984 0.967 0.946 0.920 0.983 0.883 0.847 0.840 0.901 1.054 1.010 0.987 0.987 0.990 0.875 0.844 0.990 0.875 0.845 0.949 0.977 0.890 0.875 0.898 0.867 0.868 0.867 0.846 0.811 0.754 0.692 0.665 0.741 0.977 0.977 0.997 0.9		215	.058	•	.982 0	810.	86 0.	0	95 0.	94 0.	6.0	68 0.	10.9	0 60	84 0	0 0	10.0		
160 1.035 0.989 0.975 0.974 0.976 0.978 0.973 0.959 0.933 0.898 0.866 0.863 0.921 1.063 134 1.019 0.976 0.964 0.962 0.963 0.959 0.946 0.920 0.883 0.847 0.840 0.901 1.054 110 0.997 0.957 0.946 0.944 0.940 0.928 0.901 0.861 0.821 0.810 0.873 1.042 110 0.997 0.957 0.946 0.944 0.940 0.928 0.901 0.861 0.821 0.810 0.873 1.042 110 0.997 0.957 0.946 0.944 0.940 0.928 0.901 0.861 0.821 0.811 1.024 110 0.997 0.957 0.946 0.944 0.940 0.928 0.901 0.861 0.871 1.024 110 0.997 0.957 0.901 0.895 0.875 0.845 0.796 0.742 0.770 0.837 1.024 110 0.997 0.901 0.801 0.801 0.754 0.692 0.665 0.741 0.977 110 0.997 0.901 0.801 0.801 0.801 0.801 0.801 0.801 110 0.997 0.901 0.801 0.801 0.801 0.801 0.801 110 0.997 0.901 0.801 0.801 0.801 110 0.997 0.901 0.801 0.801 0.801 110 0.997 0.901 0.801 0.801 0.801 0.801 110 0.997 0.901 0.801 0.801 0.801	160 1.035 0.989 0.975 0.974 0.976 0.978 0.973 0.959 0.933 0.898 0.866 0.863 0.921 1.063 134 1.019 0.976 0.964 0.962 0.963 0.959 0.946 0.920 0.883 0.847 0.840 0.901 1.054 110 0.997 0.957 0.946 0.944 0.940 0.928 0.901 0.861 0.871 0.873 1.042 110 0.997 0.957 0.946 0.903 0.875 0.881 0.861 0.871 0.873 1.024 110 0.998 0.991 0.991 0.916 0.903 0.875 0.832 0.786 0.770 0.837 1.024 110 0.997 0.958 0.901 0.916 0.903 0.875 0.892 0.949 110 0.993 0.901 0.996 0.815 0.944 0.796 0.742 0.720 0.793 1.003 110 0.933 0.901 0.890 0.817 0.754 0.665 0.741 0.977 110 0.898 0.866 0.576 0.514 0.514 0.692 0.682 0.949 111 0.751 0.624 0.514 0.457 0.548 0.892 112 0.900 0.801 0.801 0.801 0.801 1136 0.265 0.861	160 1.035 0.989 0.975 0.974 0.976 0.978 0.973 0.959 0.933 0.898 0.866 0.863 0.921 1.063 1.34 1.019 0.976 0.964 0.962 0.963 0.959 0.946 0.920 0.883 0.847 0.840 0.901 1.054 1.019 0.976 0.957 0.946 0.940 0.928 0.901 0.861 0.821 0.810 0.873 1.042 1.054 1.00 0.997 0.957 0.946 0.944 0.940 0.928 0.901 0.861 0.821 0.810 0.873 1.042 1.042 1.054 0.958 0.931 0.921 0.916 0.993 0.875 0.844 0.796 0.786 0.770 0.837 1.024 1.024 0.810 0.875 0.844 0.796 0.742 0.722 0.793 1.003 1.003 1.003 0.805 0.80	_	189	.047		.980	79 0.	83 0.	0	88 0.	82 0.	0.0	40 0.	6.0.8	78 0.	78 0.	- 0)		
134 1.019 0.976 0.964 0.962 0.963 0.959 0.946 0.920 0.883 0.847 0.840 0.901 1.054 110 0.997 0.957 0.946 0.944 0.940 0.928 0.901 0.861 0.821 0.810 0.873 1.042 076 0.968 0.931 0.921 0.916 0.903 0.875 0.832 0.786 0.770 0.837 1.024 031 0.933 0.901 0.890 0.875 0.844 0.796 0.742 0.722 0.793 1.003 986 0.898 0.867 0.846 0.811 0.754 0.692 0.665 0.741 0.977 0.868 0.826 0.779 0.710 0.636 0.600 0.682 0.949 974 0.854 0.751 0.624 0.514 0.457 0.531 0.617 0.920 975 0.968 0.452 0.380 0.476 0.868 976 0.394 0.305 0.403 0.851 977 0.240 0.330 0.846 978 0.265 0.861	134 1.019 0.976 0.964 0.962 0.963 0.959 0.946 0.920 0.883 0.847 0.840 0.901 1.054 110 0.997 0.957 0.946 0.944 0.940 0.928 0.901 0.861 0.821 0.810 0.873 1.042 076 0.968 0.931 0.921 0.916 0.903 0.875 0.832 0.786 0.770 0.837 1.024 031 0.933 0.901 0.890 0.875 0.844 0.796 0.742 0.722 0.793 1.003 986 0.898 0.867 0.846 0.811 0.754 0.692 0.665 0.741 0.977 9970 0.868 0.826 0.778 0.710 0.636 0.600 0.682 0.949 917 0.751 0.624 0.514 0.457 0.548 0.892 918 0.452 0.380 0.476 0.868 934 0.305 0.403 0.851 935 0.265 0.861 936 0.955 0.861 937 0.240 0.330 0.846	134 1.019 0.976 0.964 0.962 0.963 0.959 0.946 0.920 0.883 0.847 0.840 0.901 1.054 110 0.997 0.957 0.946 0.944 0.940 0.928 0.901 0.861 0.821 0.810 0.873 1.042 076 0.968 0.931 0.921 0.916 0.903 0.875 0.832 0.786 0.770 0.837 1.024 031 0.933 0.901 0.890 0.875 0.844 0.796 0.742 0.722 0.793 1.003 986 0.898 0.867 0.846 0.811 0.754 0.692 0.665 0.741 0.977 0.868 0.826 0.778 0.710 0.636 0.600 0.682 0.949 934 0.856 0.452 0.380 0.476 0.868 950 0.394 0.305 0.403 0.851 950 0.394 0.330 0.846 950 0.396 0.390 0.846 950 0.390 0.846	_	160	.035		.975 0	74 0.	76 0.	0	73 0.	59 0.	0.8	98 0.	6 0.8	63 0.	21 1.	٠. ۳	• • • • • • • • • • • • • • • • • • • •		
110 0.997 0.957 0.946 0.944 0.940 0.928 0.901 0.861 0.821 0.810 0.873 1.042 076 0.968 0.931 0.921 0.916 0.903 0.875 0.832 0.786 0.770 0.837 1.024 031 0.933 0.901 0.890 0.875 0.844 0.796 0.742 0.722 0.793 1.003 986 0.898 0.867 0.846 0.811 0.754 0.692 0.665 0.741 0.977 997 0.868 0.826 0.778 0.710 0.636 0.600 0.682 0.949 914 0.754 0.666 0.574 0.674 0.688 915 0.758 0.759 0.851 0.868 916 0.394 0.305 0.403 0.851 917 0.265 0.861 918 0.265 0.861	110 0.997 0.957 0.946 0.944 0.940 0.928 0.901 0.861 0.810 0.873 1.042 076 0.968 0.931 0.921 0.916 0.903 0.875 0.832 0.786 0.770 0.837 1.024 031 0.933 0.901 0.890 0.875 0.844 0.796 0.742 0.722 0.793 1.003 986 0.898 0.867 0.846 0.811 0.754 0.692 0.665 0.741 0.977 950 0.868 0.826 0.778 0.710 0.636 0.600 0.682 0.949 934 0.834 0.754 0.656 0.576 0.531 0.617 0.920 949 0.751 0.624 0.514 0.457 0.548 0.892 950 0.394 0.305 0.403 0.851 951 0.255 0.861 952 0.910	110 0.997 0.957 0.946 0.944 0.940 0.928 0.901 0.861 0.821 0.810 0.873 1.042 076 0.968 0.931 0.921 0.916 0.903 0.875 0.832 0.786 0.770 0.837 1.024 031 0.933 0.901 0.890 0.875 0.844 0.796 0.742 0.722 0.793 1.003 986 0.898 0.867 0.846 0.811 0.754 0.692 0.665 0.741 0.977 950 0.868 0.875 0.778 0.710 0.636 0.600 0.682 0.949 934 0.754 0.666 0.576 0.531 0.617 0.920 935 0.403 0.851 0.868 936 0.452 0.380 0.476 0.868 937 0.240 0.330 0.846 938 0.851 0.861 939 0.265 0.861	_	134	.019		.964 0	62 0.	63 0.	0	46 0.	20 0.	0.8	47 0.	6.00	01	54				
076 0.968 0.931 0.921 0.916 0.903 0.875 0.832 0.786 0.770 0.837 1.024 031 0.933 0.901 0.890 0.875 0.844 0.796 0.742 0.722 0.793 1.003 986 0.898 0.867 0.846 0.811 0.754 0.692 0.665 0.741 0.977 950 0.868 0.826 0.778 0.710 0.636 0.600 0.682 0.949 934 0.834 0.754 0.666 0.576 0.531 0.617 0.920 935 0.394 0.305 0.403 0.851 936 0.394 0.305 0.868 937 0.240 0.330 0.846 938 0.265 0.861	076 0.968 0.931 0.921 0.916 0.903 0.875 0.832 0.786 0.770 0.837 1.024 031 0.933 0.901 0.890 0.875 0.844 0.796 0.742 0.722 0.793 1.003 986 0.898 0.867 0.846 0.811 0.754 0.692 0.665 0.741 0.977 950 0.868 0.826 0.778 0.710 0.636 0.600 0.682 0.949 934 0.834 0.754 0.656 0.576 0.531 0.617 0.920 917 0.751 0.624 0.514 0.457 0.548 0.892 950 0.386 0.452 0.380 0.476 0.868 9517 0.751 0.625 0.380 0.476 0.868 9518 0.265 0.861	076 0.968 0.931 0.921 0.916 0.903 0.875 0.832 0.786 0.770 0.837 1.024 031 0.933 0.901 0.890 0.875 0.844 0.796 0.742 0.722 0.793 1.003 986 0.898 0.867 0.846 0.811 0.754 0.692 0.665 0.741 0.977 950 0.868 0.826 0.778 0.710 0.636 0.600 0.682 0.949 934 0.834 0.754 0.666 0.576 0.531 0.617 0.920 937 0.751 0.624 0.514 0.457 0.548 0.892 938 0.394 0.305 0.403 0.851 939 0.265 0.861 930 0.868	_	110	. 997	•	.946 0	44 0.	40 0.	0	010.	610.	0.8	10 0.	3	4					
31 0.933 0.901 0.890 0.875 0.844 0.796 0.742 0.722 0.7 9 3 1.0 86 0.898 0.867 0.846 0.811 0.754 0.692 0.665 0.741 0.977 0.868 0.862 0.778 0.710 0.636 0.600 0.682 0.949 0.834 0.754 0.666 0.576 0.531 0.617 0.920 0.586 0.452 0.380 0.476 0.868 0.892 0.394 0.305 0.403 0.851 0.868 0.394 0.305 0.403 0.851 0.868 0.265 0.861 0.300 0.846 0.300 0.300 0.846 0.300 0.846 0.300 0.300 0.846 0.300 0.846 0.300 0.300 0.846 0.300 0.846 0.300 0.846 0.300 0.846 0.300 0.846 0.300 0.300 0.846 0.300 0.300 0.846 0.300 0.300 0.846 0.300 0.300 0.846 0.300	31 0.933 0.901 0.890 0.875 0.844 0.796 0.742 0.722 0.793 1.086 0.898 0.867 0.846 0.811 0.754 0.692 0.665 0.741 0.977 0.868 0.886 0.826 0.778 0.710 0.636 0.600 0.682 0.949 0.751 0.654 0.574 0.666 0.576 0.531 0.617 0.920 0.586 0.452 0.380 0.476 0.868 0.892 0.394 0.305 0.403 0.851 0.868 0.394 0.305 0.403 0.851 0.868 0.395 0.390 0.394 0.305 0.403 0.851 0.868 0.265 0.861 0.846 0.394 0.305 0.403 0.851 0.851 0.395 0.3	31 0.933 0.901 0.890 0.875 0.844 0.796 0.742 0.722 0.7 9 3 1.0 86 0.898 0.867 0.846 0.811 0.754 0.692 0.665 0.741 0.977 50 0.868 0.826 0.778 0.710 0.636 0.600 0.682 0.949 34 0.834 0.754 0.666 0.576 0.531 0.617 0.920 17 0.751 0.624 0.514 0.457 0.548 0.892 90 0.586 0.452 0.380 0.476 0.868 60 0.394 0.305 0.403 0.851 57 0.240 0.330 0.846 98 0.265 0.861 17 0.910	_	920	968		.921 0	16 0.	03 0.	0	32 0.	86 0.	0	37 1.	24			بم			
86 0.898 0.867 0.846 0.811 0.754 0.692 0.665 0.741 0.977 50 0.868 0.826 0.778 0.710 0.636 0.600 0.682 0.949 34 0.834 0.754 0.666 0.576 0.531 0.617 0.920 17 0.751 0.624 0.514 0.457 0.548 0.892 90 0.586 0.452 0.380 0.476 0.868 60 0.394 0.305 0.403 0.851 57 0.240 0.330 0.846 15 0.910	86 0.898 0.867 0.846 0.811 0.754 0.692 0.665 0.741 0.977 50 0.868 0.826 0.778 0.710 0.636 0.600 0.682 0.949 34 0.834 0.754 0.666 0.576 0.531 0.617 0.920 17 0.751 0.624 0.514 0.457 0.548 0.892 90 0.586 0.452 0.380 0.476 0.868 60 0.394 0.305 0.403 0.851 57 0.240 0.330 0.846 15 0.910	86 0.898 0.867 0.846 0.811 0.754 0.692 0.665 0.741 0.977 50 0.868 0.826 0.778 0.710 0.636 0.600 0.682 0.949 34 0.834 0.754 0.666 0.576 0.531 0.617 0.920 17 0.751 0.624 0.514 0.457 0.548 0.892 90 0.586 0.452 0.380 0.476 0.868 60 0.394 0.305 0.403 0.851 57 0.240 0.330 0.846 15 0.910	_	31	. 933		.890	75 0.	44 0.	o.	42 0.	22 0.	-0	03				1			
50 0.868 0.826 0.778 0.710 0.636 0.600 0.682 0.94 34 0.834 0.754 0.666 0.576 0.531 0.617 0.920 17 0.751 0.624 0.514 0.457 0.548 0.892 90 0.586 0.452 0.380 0.476 0.868 60 0.394 0.305 0.403 0.851 57 0.240 0.330 0.846 15 0.910	50 0.868 0.826 0.778 0.710 0.636 0.600 0.682 0.94 34 0.834 0.754 0.666 0.576 0.531 0.617 0.920 17 0.751 0.624 0.514 0.457 0.548 0.892 90 0.586 0.452 0.380 0.476 0.868 60 0.394 0.305 0.403 0.851 57 0.240 0.330 0.846 98 0.265 0.861 17	50 0.868 0.826 0.778 0.710 0.636 0.600 0.682 0.94 34 0.834 0.754 0.666 0.576 0.531 0.617 0.920 17 0.751 0.624 0.514 0.457 0.548 0.892 90 0.586 0.452 0.380 0.476 0.868 60 0.394 0.305 0.403 0.851 57 0.240 0.330 0.846 15 0.910	Ċ.	98	888	•	.846	1100	54 0.	Ö	65 0.	41 0.						c			
34 0.834 0.754 0.666 0.576 0.531 0.617 0.92 17 0.751 0.624 0.514 0.457 0.548 0.892 90 0.586 0.452 0.380 0.476 0.868 60 0.394 0.305 0.403 0.851 57 0.240 0.330 0.846 98 0.265 0.861 15 0.910	34 0.834 0.754 0.666 0.576 0.531 0.617 0.92 17 0.751 0.624 0.514 0.457 0.548 0.892 90 0.586 0.452 0.380 0.476 0.868 60 0.394 0.305 0.403 0.851 57 0.240 0.330 0.846 98 0.265 0.861 17	34 0.834 0.754 0.666 0.576 0.531 0.617 0.92 17 0.751 0.624 0.514 0.457 0.548 0.892 90 0.586 0.452 0.380 0.476 0.868 60 0.394 0.305 0.403 0.851 57 0.240 0.330 0.846 98 0.265 0.861 15 0.910	\sim	20	868	٠	. 778	10 0.	36 0.	Ö	82 0.	4		,						,	
17 0.751 0.624 0.514 0.457 0.548 0.892 90 0.586 0.452 0.380 0.476 0.868 60 0.394 0.305 0.403 0.851 57 0.240 0.330 0.846 98 0.265 0.861 15 0.910	17 0.751 0.624 0.514 0.457 0.548 0.892 90 0.586 0.452 0.380 0.476 0.868 60 0.394 0.305 0.403 0.851 57 0.240 0.330 0.846 98 0.265 0.861 15 0.910	17 0.751 0.624 0.514 0.457 0.548 0.892 90 0.586 0.452 0.380 0.476 0.868 60 0.394 0.305 0.403 0.851 57 0.240 0.330 0.846 98 0.265 0.861 15 0.910	Ċ.	34	.834		999	76 0.	310.	0	2										
90 0.586 0.452 0.380 0.476 0.868 60 0.394 0.305 0.403 0.851 57 0.240 0.330 0.846 98 0.265 0.861 15 0.910	90 0.586 0.452 0.380 0.476 0.868 60 0.394 0.305 0.403 0.851 57 0.240 0.330 0.846 98 0.265 0.861 15 0.910	90 0.586 0.452 0.380 0.476 0.868 60 0.394 0.305 0.403 0.851 57 0.240 0.330 0.846 98 0.265 0.861 15 0.910	~	17	.751		514	57 0.	48 0.												
60 0.394 0.305 0.403 0.851 57 0.240 0.330 0.846 98 0.265 0.861 15 0.910	60 0.394 0.305 0.403 0.851 57 0.240 0.330 0.846 98 0.265 0.861 15 0.910	60 0.394 0.305 0.403 0.851 57 0.240 0.330 0.846 98 0.265 0.861 15 0.910	~	90	.586		.380	76 0.	89												
57 0.240 0.330 0.846 98 0.265 0.861 15 0.910	57 0.240 0.330 0.846 98 0.265 0.861 15 0.910	57 0.240 0.330 0.846 98 0.265 0.861 15 0.910	_	09	394		403	بر ب		ż						•					
98 0.265 0.861 15 0.910	.215 0.910		· ~	357	240		846)		۰.,											-
15 0.910 17	15 0.910	15 0.910	٠.	, a	265	•	5														
17	.017	.017	\ ^		0.00					٠.											
-	<u>-</u>	5		2 7	D																
			_	5									•								

HITTALL 1. 95 - 85 - 75 - 65 - 15 - 45 - 15 - 45 - 15 - 15 - 15 - 1			1	1	1
HETA-1 OF STATE OF ST					
#FTF1-100 THET 1-700 THET 1-700 THE TA-2 T	•			10	74 4 7 6 9 5 5 6 7 7 9 7 9 7 9 7 9 7 9 9 9 9 9 9 9 9 9
THE A TO SET THE STATE OF THE S					7 to 2 to 3 to 3 to 4 to 4 to 4 to 4 to 4 to 4
HETA-1 - 95 - 75 - 75 - 75 - 75 - 75 - 75 - 75					87.7.0
HITT- 20 HIT					00 00 00 00 00 00 00 00 00 00 00 00 00
HITA-120 HITA-20 HITA-		,			
HETA-1 190 9 500 15 175 - 65 - 25 - 45 - 35 - 15 - 15 - 05 05 15 25 35 - 45 5 45 5 1 11111					100 00 00 00 00 00 00 00 00 00 00 00 00
HETA-1 195					- 000000 - 000000
HETA-1 190 9 530 1151 120 1151 120 9 530 1151 120 9 530 1151 120 9 530 1151 120 9 530 1151 120 120 9 530 120 130 130 130 130 130 130 130 130 130 13					······································
HETA-1 - 95 - 85 - 75 - 65 - 56 - 45 - 35 - 75 - 15 - 05 - 15 - 25 - 31 - 45 - 35 - 75 - 15 - 05 - 05 - 15 - 25 - 31 - 45 - 35 - 75 - 15 - 05 - 05 - 15 - 25 - 31 - 31 - 31 - 31 - 31 - 31 - 31 - 3					
HETA-1 1 - 95 - 89 - 75 - 65 - 35 - 45 - 35 - 25 - 15 - 05 05 15 25 HETA-1 1 0 0 1 5 5 0 1 1 1 1 1 1 1 1 1 1 1 1 1					
HETA-1 19 5-30 HETA-2 HETA-2 HETA-2 HETA-2 HETA-2 HETA-3 HETA-2 HETA-3 HETA-4 HETA-3 HE				10	669 600 600 600 600 600 600 600 600 600
HETA-1 HETA-1 HETA-1 HETA-2 HETA-2 HETA-3 HETA-3 HETA-4 HETA-1 HETA-2 HETA-1 HETA-2 HETA-2 HETA-3 HETA-3 HETA-4 HETA-1 HETA-1 HETA-1 HETA-2 HETA-1 HETA-2 HETA-2 HETA-2 HETA-3 HETA-2 HETA-3 HETA-4 HETA-3 HETA-4 HETA-5 HETA-6 HETA-6 HETA-7					
HETA-1 HETA-1 HETA-2 HETA-1 1. 95				15	
HETA-1 1 90		1 -		·	
HETA-1 HETA-1 HETA-1 HETA-1 95857565554535251506 HETA-1 190 9 530 8 477 8 741 190 9 530 1 100 1 223 1 375 1 20 1 2 23 1 3 2 2 2 3 2 3 2 3 2 3 2 3 3 3 3		-		.05	A 0 0 0 0 0 0 0 0 0 0 0 0
HETA - 1 9 5 330 1 90 6 34 5 6 10 1 78 4 1 10 1 1 12 1 1 12 1 1 13 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	е	МАРХ		10	66 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
HETA-1 190 9.530 1.05 9.530 1.00	Ľ.	ш.		9.	
HETA-1 190 9.530 1.05 1.05 1.06 1.07 1.00	ŽI QN		l ⊢		
HETA-1 190 9.530 1.05 1.05 1.00 9.530 1.00 1.00 1.00 9.530 1.00 1.	APPE	CIE	THE.	ı.	i i
HETA-1 190 9 530 1100 9 530 1110 1100 9 530 9 530 1110 110 110 110 110 110 110 110 110 110 110 110 110 110 11		1 44			m00000000000000000000000000000000
HETA-1 -	¦ >		ر ب	4 8 8 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
HETA-1 958575655545 1 90		LAT	:	6.	
HETA-1 9585756555 HETA-1 1.90 9.530 1.80 1.40 1.		3 ×			
HETA-1 1. 90 9. 530 1. 90 1. 90 9. 530 1. 90 9. 530 1. 10				,	· · · · · · · · · · · · · · · · · · ·
HETA-1 1.90 9.530 1.40 1.50 6.454 6.044 7.154 6.611 7.154 6.611 7.154 6.611 7.154 6.611 7.154 7.154 7.154 7.154 7.154 7.154 7.154 7.154 7.154 7.154 7.154 7.154 7.157 7.157 7.158 7.159 7.150 7.159 7.150 7.150 7.150 7.151 7.150 7.15				ស	
HETA-1 1.90 9.530 1.20 1.90 9.530 1.40 1.50 9.530 1.20 1.40 9.530 1.20 1.30 1.40 9.530 1.20 1.30 1.20 1.30 1.20 1.30 1.30 1.20 1.30 1.30 1.30 1.30 1.30 1.30 1.30 1.3					252 262 272 272 273 273 273 273 273 27
HETA-1 1.90 9.530 1.70 1.70 1.70 1.70 1.70 1.70 1.70 1.7		ļ		9.	The state of the s
HETA-1 95857 HETA-1 95857 1.90 9.530 1.40 8.477 8.741 1.50 6.454 5.094 4 1.40 8.477 8.722 1.40 4.025 2.358 1.10 4.025 2.358 1.10 3.009 1.722 0.50 3.780 1.975 1.00 3.780 1.975 1.00 3.780 1.975 1.00 3.780 1.975 1.00 3.780 1.975 1.00 3.780 1.975 1.00 3.780 1.975 1.00 3.780 1.975 1.00 1.00 2.130 1.290 1.00 1.00 2.130 1.290 1.00 1.00 1.250 1.102 0.00 0.00 1.542 1.039 1.10 1.25 0.881 1.20 1.255 0.881 1.20 0.676 0.477 1.20 0.676 0.477 1.20 0.676 0.477 1.20 0.676 0.477 1.20 0.676 0.487 1.20 0.683				LS.	8 0 2 5 7 6 7 7 8 9 8 9 2 7 7 7 8 9 8 9 2 7 7 7 8 9 7 8 9 8 9 2 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
HETA-1 9585 HETA-1 9585 HETA-1 9585 9595 95 -				7	<u> </u>
HETA-1 HETA-1 1.90 9.530 1.40 1.70 1.50 1.70 1					7.00-00-00-00-00-00-00-00-00-00-00-00-00-
HETA-1 HETA-1 BO	~				
HETA-1 1 20 1 1 20 1 2					+ $ -$
HETA-				1	
	-		7	₹	000000000000000000000000000000000000000
				ш u	

	-			· · · · · · · · · · · · · · · · · · ·	
	. ``	-	95	88.0	*
,			,	60 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
			85	000	
				884 791 707 658 841	
			75	00000	
	-			022 920 8873 8873 8873 8873 827	
¥.			. 65	-00000 mon m m 0 /	
4			ľo.	138 980 980 988 888 888 651 651 7	
			55	666 663 663 663 663 663 663 663 663 663	
			5,	200000000000000000000000000000000000000	
			4	7 4 2 3 4 5 5 6 3 5 6 5 6	
			35	+ + + 00000000000000000000000000000000	
		, , ,	· .	624 0055 0055 0090 0990 0998 0978 0958 0974 1470	
			25		
				884 0015 0015 0015 0015 0017 0017 0017 0017	
1	S		15	++++0000000000	
	10 0			219 132 132 133 133 134 135 136 137 137 137 137 137 137 137 137 137 137	
	01 X		.05	7 4 2 8 0 9 W W W W W W W W W W W W W W W W W W	
4	MAP		, 05	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
u.	0 F		0.	00 00 00 00 00 00 00 00 00 00 00 00 00	
APPENDIX	ENCY	ra-2	ا 5	3 2 0 3 3 2 0 3 3 2 0 3 3 2 0 3 3 2 0 3 3 2 0 3 3 3 2 0 3 3 3 2 0 3 3 3 2 0 3 3 3 2 0 3 3 3 3	•
PPE	ICIEN	THE.	i i	00000000000000000000000000000000000000	
₹	<u>u.</u>		25		
	VE E		i i	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	
	ATI		35	, 4000000000000000000000	
	REL		. 1	79 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	
,			45	2027 8 - 620 8 8 0 0 7 2 8 - 6 2 9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
			2	40 8 1 2 4 4 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1	
			ر د	777777777777777777777777777777777777777	
			65	504 504 604 604 604 604 604 604 604 6	
			,	m m n 0 0 0 0 0	
			ري د	200 200 201 201 201 201 201 201 201 201	
			r7	000000000000000000000000000000000000000	
			85	10000000000000000000000000000000000000	
			i	5 m m 4 u u u u u u u u u u u u u u u u u	
			95	00000000000000000000000000000000000000	-
			ı	6-08-08-08-04-4-08-08-09-09-09-09-09-09-09-09-09-09-09-09-09-	•
		30	-	<u> </u>	-
		31	ETA	00000000000000000000000000000000000000	
!		_	THE		-

			. 95	0 709		
•	3		85	0.705		
			75	0.916 0.826 0.587 0.587	5	s.:
			65	1 029 0 942 0 943 0 738 0 666		
		¥	55	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
			45	0.9994 0.9984 0.959 0.959 0.959 0.658	- "	
				331 0000 0000 0000 0000 0000 0000 0000		,
			. 3	4 86 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9		
			5 . 2	60000000000000000000000000000000000000		
	0 015		гō -	969 969 969 969 969 969 969 969		
വ	MAPX T		0.	347 137 137 137 137 137 137 137 137 137 13		,
DIX ≮.	CY OF	A-2	50	2 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		
APPEND	F I ĜI ENC	THET	5 1	7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	* 1	4
	IVE EF		5 - 2	## + + + + + + + + + + + + + + + + + +		•
,	RELAT		5 - 3	8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	· ·	
	,		54	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		
			55	068 068 068 068 068 068 068 068	0	
		,	9	0.6.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.	9 4 10 10 9 0 0	
			75	6.00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0000	
	ı		85	7. 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	. 78 . 61 . 61 . 16	
					1,319 1,077 0,407 0,102	
	-	n = 50	THE TA-1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	60 60 60 60 60 60 60 60 60 60 60 60 60 6	

	- 	1	1	9
			95	0 1
				779 592 487
			. 85	-8408 000
, -			LC .	95 95 74 74 74 74 74 74 74 74 74 74 74 74 74
				9010 9010 9010 9010 9010 9010 9010
			65	
	`			00000000000000000000000000000000000000
			. 55	-0000000
				000 000 000 000 000 000 000 000 000 00
		·	. 45	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	-		ស៊ី	= 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
المعياد. و	٧		€.	7.77 0018 0018 0018 0018 0018 0018 0018 00
			25	
in.				4 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	S		. 15	++++00+0000000
	0 01	r	rs S	0000 0000 0000 0000 0000 0000 0000 0000 0000
	×		Ö.	ων ν 4 δω π ω ω δ δ δ ω π 4 π 4 4 ± π ω 000 + + + 00000000
9	MAP		05	1.839 1.004 1.004 1.0000 1.0000
×	0.5	2	-	77777777777777777777777777777777777777
APPENDI	ENCY	ĒTA-	. 15	N000000000000000000000000000000000
APP	101	THE	ı	80000000000000000000000000000000000000
	E1.F	(25	N+++++00000000000000000000000000000000
	IVE	/	r.	86.5-6.0000000000000000000000000000000000
	ELAT		E	0048 0048 0044
	a a		45	
			,	1900 1900 1900 1900 1900 1900 1900 1900
		_	. 55	F 4 0 0 0 0 0 0 0
\		,	1 :	5521 7031 7031 7031 7031 7031 7031 7031 703
·			- 65	04
			,	88 987 987 987 987 988 988 988 988 988 9
1.			75	m44444444444444444444460000000000000000
			5	C 2 3 0 7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
			60	4 @ R @ C C C C C C C C C C C C C C C C C
			95	, 200 ,
			9,	0000000000440000444044044004 000000000447474-0700404-000007044004-004
		8		
		6	ETA	98799746679688799696969696969696969696969696969
	<u> </u>	С	<u> </u>	

	1	ı	1	000
	•		95	86 O
	18		3	833 777 6
	"		85	
			" .	8 1 8 8 7
			5	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
			,	8 8 7 - 9 - 8
		do.	ľĎ.	8 0 0 0 0 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9
			9.	600000 000000
		,54	2	8.00.00.00.00.00.00.00.00.00.00.00.00.00
			.5	0000000
			2	80000000000000000000000000000000000000
		,	4.	00000000
			S.	
			Ř.	
			r.	709 8857 9997 9997 788 788
			.2	000000-000000
				656 656 930 990 990 990 990 990 990 990 990 990
	×		15	000000000000
	MAP		_ ,	604 604 604 605 605 605 605 605 605
	10		0.5	000000000000000000000000000000000000000
	GLS			555 7 155 7
ن +	и_		رَ	000000000000000000000000000000000000000
×I	λ 0	-2	1	508 658 658 8891 736 600 600 600 600 600 600 600 600 600 6
END I X	ENC	ETA	15	00000000000000
APP	ICI	Ŧ	1	4666 735 999 999 999 999 999 999 999 999 999 9
,	EFF		25	000000000000000000000000000000000000000
	VE I		,	4411 6689 6688 6688 6688 6688 6689
	ATI	i	. 35	
	REL/		1	100 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	-		45	
-			ı'	ω α α α α α ά 4 ά τι α ω τι
,			55	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
			'	000000000000000000000000000000000000000
			65	353 353 353 353 353 353 353 353 353 353
			i i	000000000000000000000000000000000000000
			TU.	7.73 7.73 7.73 7.73 7.73 7.73 7.73 7.73
			77	00000000000000000000000000000000000000
			2	ñ Ô n m ± m m r ü ± 0 ± 0 ± 0 0 m m 4 ü u u 4 u ± n ü n m u n u t = e.u 0 ±
			88	6 6 6 6 7 7 7 7 8 8 8 8 8 8 8 8 8 8 8 8
	,			000000000000000000000000000000000000000
	:		. 95	- E E E E E - C 4 7 - C E E E E E E E E E E E E E E E E E E
				00000000000000000000000000000000000000
		5	-	
		н	ETA	98 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
		5	THE	

			2	999
			6	849 766 0 667
_		0	85	6 0 - 4 8
		/	75	0 0 9 4 0 0 9 1 0 0 6 6
				9943 9943 9963 9963 9963 9963 9963
			.65	96 777 0. 770 0. 730 0. 59 0. 59 0.
**			55	00.097 00.093 00.093 00.093 00.093
	_			8 2 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
			. 45	24 99 99 99 99 99 99 99 99 99 99 99 99 99
-			.35	
			5	654 654 654 656 656 656 656 656 656 656
			. 2	557 557 557 557 557 557
•	×		. 15	, 000000000000
	O MAP		92	0.489 0.783 0.992 0.993 0.993 0.998 0.998 0.998 0.998 0.950 0.970 0.950 0.950
	LS TO			7 4 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
6.2	OF G		05	00000000000000
PPENDIX	ENCY	TA-2	15	0 0 362 0 0 980 0 0 991 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
APPE	ICI	THE	5	3123 3273 3273 3273 3273 3273 3273 3273
	E EFF		- 25	7 8 4 7 4 7 4 7 7 7 7 7 7 7 7 7 7 7 7 7
	ATIV		. 35	
	REL		5	2447 2447
			. 4	222 222 223 2424 2544 2544 2544 2544 254
			55	00000000000000000000000000000000000000
			. 65	2006 2006 2006 2006 2007 2009 2009 2009 2009 2009 2009 2009
•				
			. 75	193 193 193 193 193 193 193 193 193 193
			85 -	639 00 00 00 00 00 00 00 00 00 00 00 00 00
-				2,4,4,6,6,4,4,4,0,0,0,0,0,0,0,0,0,0,0,0,0
-		,	- 95	7 1 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3
,		0	- . i	000000000000000000000000000000000000000
		#	HETA-	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
		ַ	F-+	

				111	-
			5	48	
			6.	4 8 8 4 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
Ļ			.85	000	
			75	0 944 0 936 0 962 0 488	
			, 17	920 982 0 947 0 721 0 489	
			. 65	00000	
			.55	0 .00 .00 .00 .00 .00 .00 .00 .00 .00 .	
			S	778 968 994 995 995 963 963	
		,	4.	69 69 99 89 99 99 99 99 99 99 99 99 99 99 99	
			35		
			52	599 995 995 999 999 999 999 999 999 999	
			. 2	513 990 900 900 900 900 900 900 90	
	×		. 15	0000000000000	
	O MAPX		05	0. 934 0. 934	
၉	OF GLS T		īῦ	364 773 921 921 938 938 939 937 941 342 342	
ن		2	0.	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	
APPENDIX	ENCY	T A -	. 15		
(APP	FFICIENC	1.E	5 -	255 900 900 900 900 900 900 900 9	
	ш		2	11 1 2 4 0 4 8 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	-
	LATIV		35		
	REL		45	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
			ı	7 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	
	-		55		
			. 65	137 137 137 137 137 137 137 137 137 137	
			,	- 400	
	٠	¥),	75	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	*· ,
, ja			85	00 00 00 00 00 00 00 00 00 00	* :
			5	, 000000000000000000000000000000000000	
	:		36 · -	000 1120 1	
		20	A - 1	000000000000000000000000000000000000000	
		e c	THE T.	1	
			·		

ŝ

				, · · · · · · · · · · · · · · · · · · ·
			95	9
); 	m O 80
			85	78.00.70
			~	949 955 720 413
			75	00000
			· Sade	9 9 18 9 9 8 4 9 9 6 3 9 9 6 3 4 1 7 4 0 0 4 1 7 4 0 0 4 1 7 7 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
			65	000000000000000000000000000000000000000
				8857 9867 9986 9987 757 757
			55	0000000
			•	782 997 997 772 772 414
			45	00000000000
			•	698 9993 9993 9993 9994 784 406
-			35	000000000000
				611 987 993 993 993 993 993 393 393 393
			. 25	00000000000
				5526 9913 9913 9913 9913 9913 9913 9913 991
	×		. 1 5	00000000000
	MAP)	~		4445 9965 9966 9996 9996 9999 9999 9994 350
	10 %		.05	000000++++++000000
,	۲S			37.1 99.7 99.7 99.7 99.7 99.7 99.8 99.8 32.1 32.1
6.4	n G		.05	00000000000000
×	٥ ج	-2		306 746 995 995 995 995 995 995 995 99
APPENDI	ENC	НЕТА	. 45	
APP	101	‡	ı,	255 657 657 657 657 657 657 657 6
	EFF		. 2	0000000000000000
	IVE		r.	202 203 203 203 203 203 203 203
	LAT		6	80 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	RE		L)	6 4 4 6 7 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
			4.	000000000000000000000000000000000000000
		۵	លី .	8 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
			ا . ت	000000000000000000000000000000000000000
			ις.	100 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
			9.	
			10	8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
•			. , 75	
			10	Φ Φ Φ ω 4 4 Φ 4 - L Φ ω 9 ω ω L Φ Φ Φ Φ ω Φ ω Φ ω Φ ω Φ ω Φ ω Φ ω
			85	0 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0
			. 95	0699 0882 0882 0882 0882 0882 0882 0882 08
				000000000000000000000000000000000000000
		3	-	000000000000000000000000000000000000000
	-	" C	HETA	++++++++++++++++++++++++++++++++++++++
			<u></u>	

		ļ			
		-	. 95	∑ 10 4 4	•
*			Ω	0.91	
	,	*		959 973 787 364	•
,		₩	. 75	931 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
			. 65	စ်စ်စ်စ်စ်စ်စ စုဝဝဝဝဝ	
			ഗ	88 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
			<u>.</u>	8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	
,			. 45	00000000	
1				9.000 9.000	
			e,	6 7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
!			. 25	000000000	
			15	0 0 98 9 0 0 0 98 9 0 0 98 9 0 0 98 9 0 0 98 9 0 0 98 9 9 9 9	
	MAPX	`	· .	9914 0 000 000 000 000 000 000 000 000 000	
	101		.05	000000000000	
rō.	GL S	,	05	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
IX G	Y 0F	2	, ,	3445 0000	
APPENDÍX	1 ENC	НЕТА	- , 15	2746 7300 9889 9983 9983 9993 9993 9993 9993 9	
AP	FFIC	-	.25	, 0000000000000000000000000000000000000	
	IVE		LC)	6000 6000 6000 6000 6000 6000 6000 600	
	ELAT	•	 36	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
	α		. 45		
		:	LC .	7	
		·	ا . ت	000000000000000000000000000000000000000	
			, 65	0.097 0.	
				744 747 748 749 749 749 749 749 749 749 749	
			75	00000000000000000000000000000000000000	
			85	057 157 157 157 157 157 157 157 157 157 1	
			ر ا		
			6 -	044 056 070 085 085 085 085 085 085 085 08	
		50	-		
		"	THETA	00000000000000000000000000000000000000	
	l 	<u> </u>	l F		

	ı	į.	1	200
			95	m.
			0,	0 0 0
			ر ما . ما	, 37, 37, 37, 37, 37, 37, 37, 37, 37, 37
			80	000
				9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
			75	00000
				99999999999999999999999999999999999999
			65	000000
				38 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
			55	
				8889 9993 9993 9997 9977 56
		ŀ	. 2	
		١.		
			2	840 988 998 999 999 924 977
			6	-0000000000000000000000000000000000000
			ري ا - ي	78 1 980 999 999 999 999 999 999 485
			25	000000000
			-	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
	\ ×		5.	00000000000
	MAP			0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	0		05	
	ST			8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
)	5		05	
3	9.	2		
)	Ž,	Α-	2	
	IENC	H H		4 n 0 4 r u n a a a a a a a a a a a a a a a a a a
	FIC	-	L L	354 825 939 939 939 939 939 939 939 939 939 93
	EF	`-	2	000000000
	IVE			269 951 995 995 995 999 999 999 999 999 99
	AT		35	000000000000000000000000000000000000000
	REL		٠.	196 196 196 196 196 196 196 196 196 196
			4.5	, 0000000000000000000000000000000000000
•		. (1	138 1481 1712 1712 1933 1947 198 199 199 199 199 199 199 199 199 199
_		1	55	41-2200000000000000000000000000000000000
			i i	
			65	2000 2000
	,			
			. 75	0.000000000000000000000000000000000000
			ł	
			85	040 170 170 170 170 171 171 171 17
			ı'	
			95	
			0,	025 038 038 112 112 112 112 113 113 113 113 113 113
		8		000000000000000000000000000000000000000
		5	A - 1	
		.	HET	90 10 10 10 10 10 10 10 10 10 1
	!	C	F	7777777777799999999999999

APPENDIX G 6

APPENDIX H.1

C**** This FORTRAN program is to be use to obtain the transformed

```
C**** variables, to perform the EGLS and can also be use as a sub
C**** -routine for ML, when the Regression Model has MA(2) Errors.
    - REAL*8 TH(2),YT(10),XTO(10),XT(10),S(10,10)
      REAL*8 YST(10), XST1(10), XST2(10), A11, A12, A13
C**** TH's are the two MA prameters reading from MTS file.
C**** YT, XTO, XT are the dependent variable and two independent
C**** variable, one of them may be column of 1's for intercept.
C**** S is the square root matrix of covariance matrix V.
C**** YST, XST1, XST2 are the transformed variables of YT, XTO, XT.
      INTEGER N,M,I,L,J,K
      N = 10
C**** This N is for sample size, to be changed, when necessary.
      READ (3,60) TH
      READ (5,60) YT
      READ (2,58) XTO
      READ (4,60) XT
      A11=1.0+TH(1)*TH(1)+TH(2)*TH(2)
      A12 = -TH(1) * (1.0 - TH(2))
      A 1 3 = -TH(2)
      S(1,1)=A11**.5
      YST(1) = YT(1) / S(1,1)
      XST1(1)=XTO(1)/S(1,1)
      XST2(1) = XT(1)/S(1,1)
      S(1,2)=A12/S(1,1)
      S(2,2)=(A11-S(1,2)*S(1,2))**.5
      YST(2) = (YT(2) - S(1,2) * YST(1)) / S(2,2)
      XST1(2) = (XTO(2) - S(1,2) * XST1(1)) / S(2,2)
      XST2(2) = (XT(2) - S(1,2) * XST2(1)) / S(2,2)
      K = 1
      L=2
C**** The values given to K and L are fixed, not to be changed.
      DO 10 J=3,N
      S(K,J) = A13/S(K,K)
      S(L,J) = (A12-S(L-1,J-1)*S(L-1,J))/S(L,L)
      S(J,J)=(A11-S(K,J)*S(K,J)-S(L,J)*S(L,J))**.5
      YST(J) = (YT(J) - S(L,J) * YST(J-1) - S(K,J) * YST(J-2)) / S(J,J)
      XST1(J) = (XTO(J) - S(L,J) * XST1(J-1) - S(K,J) * XST1(J-2)) / S(J,J)
      XST2(J) = (XT(J) - S(L,J) * XST2(J-1) - S(K,J) * XST2(J-2)) / S(J,J)
      K = K + 1
      L=L+1
      CONTINUE
10
      WRITE (6,10025) YST
      WRITE (7,10025) XST1
      WRITE (8,10025) XST2
C**** These transformed variables may be used for EGLS.
10025 FORMAT(F16.8)
58
      FORMAT(F3.0)
60
      FORMAT(F9.5)
      STOP
      END
```

J. 6. F.

APPENDIX H.2

```
This program will calculate the exact determinant of
      covariance matrix \Omega for MA(2) error process using \theta matrix.
      REAL*8 A1(50,3),SA1,SA2,SA3,DET,THETA(2),Z1(50),Z2(50)
      READ (5,100) THETA
C***
      Where THETA is for moving average parameters.
      MM = 50
C***
      Where MM is the sample size, change when necessary along
C***
      with the dimensions specified above.
      Z1(1) = -1 * THETA(1)
      Z2(1) = -1 * THETA(2)
      A1(1,1)=Z1(1)*Z1(1)
      A1(1,2)=Z2(1)*Z2(1)
     A1(1,3)=Z1(1)*Z2(1)
      SA1 = A1(1,1)
      SA2 = A1(1,2)
      SA3=A1(1,3)
      DO 115 I = 2, MM
      Z1(I) = THETA(1) * Z1(I-1) + Z2(I-1)
      Z2(I) = THETA(2) * Z1(I-1)
      A1(I,1)=Z1(I)*Z1(I)
      A \uparrow (I,2) = Z2(I) * Z2(I)
      A1(I,3)=Z1(I)*Z2(I)
      SA1 = A1(I,1) + SA1
      SA2=A1(I,2)+SA2
115
      SA3 = A1(I,3) + SA3
      DET = (1+SA1)*(1+SA2)-(SA3)*(SA3)
      WRITE(6,121) DET
121
      FORMAT(F10.3)
100
      FORMAT(F12.8)
      STOP
      END '
```

BIBLIOGRAPHY

- Aigner, D.j. (1971). A compendium of estimation of the autoregressive moving average model from time series data, International Economic Review. 12, 348-371.
- Ali, M.M. and Thalheimar, R. (1983). Stationary tests in time series model, Journal of Forecasting, vol.2, 249-257.
- Ansley, C.F. (1979). An algorithm for the exact likelihood of a mixed autoregressive-moving average process, Biometrika, 66,1, 59-65.
- Balestra, P. (1980). A note on the exact transformation associated with the first-order moving average process, Journal of Econometrics, 14, 381-394.
- Beach, C.M. and MacKinnon, J.G.(1978). A maximum likelihood procedure for regression with autocorrelated errors, *Econometrica*, 46, 51-58.
- Beguin, J.-M., Gourieroux, C. and Monfort, A. (1980).

 Identification of a mixed autoregressive-moving average process: The corner method, *Time Series*. Amsterdam:

 North-Holland publishing company, 423-436.
- BMDQ2T,(). BMDQ2T TSPACK, Health sciences computing facility, University of California, LA, CA 90024.
- Box, G.E.P. and Jenkins, G.M. (1970). Time Series Analysis Forecasting and Control, San Francisco: Holden Day.
- Box, G.E.P. and Jenkins, G.M. (1976). Time Series Analysis Forecasting and Control, San Francisco: Holden Day.
- Box, G.E.P. and Pierce, D.A.(1970). Distribution of residual autocorrelation in autoregressive-integrated moving average time series models, Journal of American Statistical Association, 65, 1509-1526.
- Choudhury, A.H. and Chaudhury, M.M. (1984). A note on approximate estimator for the first-order moving average process, *Journal of Econometrics*, (submitted).
- Durbin, J. (1970). Testing for serial correlation in least squares regression when some of the regressors are lagged dependent variables. *Econometrica*, 38, 410.
- Durbin, J. and Watson, G.S. (1950). Testing for serial correlation in Least Squares Regression I, Biometrika, 37, 409-428.

- Durbin, J. and Watson, G.S.(1951). Testing for serial correlation in Least Squares Regression II, Biometrika, 38, 159-178.
- Fuller, W.A. (1976). Introduction to Statistical Time Series, New York: Wiley.
- Goldberger, A.S. (1963). Econometric Theory, New York: Wiley,
- Granger, C.W.J. (1980). Forecasting in business and economics, New York: Academic Press.
- Harvey, A.C. (1981). The Econometric Analysis of Time Series, London: Philip Allan.
- Johnston, J. (1972). Econometric Methods. New York: Wiley, MacGraw-Hill.
- Judge, G.G., Griffiths, W.E., Hill, R.C. and Lee, T.-C. (1980). The Theory and Practice of Econometrics, New York: Wiley.
- Kendall, Sir.M., Stuart, A. and Ord, J.K. (1983), vol.3., The Advanced Theory of Statistics, London: Griffin.
- Ljung, G.M. and Box, G.E.P. (1978). On a measure of lack of fit in time series model, Biometrika, 65, 297-303.
- MacDonald, G.M. and MacKinnon, J.G. (1985). Convenient methods for estimation of linear regression models with MA(1) errors, Canadian Journal of Economics, XVIII, no.1, 106.
- McLeod, A.I. (1977). Improved Box-Jenkins estimators, Biometrika, 64, 531-534.
- MINITAB, (1982). MINITAB Reference Manual, Statistics department, 215 pond laboratory, The Pennsylvania State University, pa. 16802.
- NAG, (1982). NAG Library Manual, Numerical Algorithms Group, Mayfield House, 256 Banbury Road, Oxford, Ox2 7DE, UK.
- Nicholls, D.F., Pagan, A.R. and Terrel, R.D. (1975), The estimation on and use of models with moving average disturbance terms:

 A Survey, International Economic Review, 16, 113-134.
- Osborn, D.R.(1976). Maximum Likelihood estimation of moving average process, Annals of Economic and Social measurement, 3, 75-87.
- Pagan, A. (1973). Efficient estimation of models with composite disturbance terms, Journal of Econometrics, 1, 329-340.

- Pagan, A. (1974). A Generalized approach to the treatment of autocorrelation, Australian Economic papers, 13, 267-280.
- Pagan, A.R. and Nicholls, D.F. (1976). Exact Maximum Likelihood estimation of regression models with finite order moving average errors, Review of Economic Studies, 43, 383-388.
- Park, C.Y. and Heikes, R.G. (1983). A note on Balestra's (1980) approximate estimator for the first-order moving average process, Journal of Econometrics, 21, 387-388.
 - Pesaran, M.H. (1973). Exact maximum likelihood estimation of a regression equation with a first-order moving average errors, Review of Economic Studies, 40, 529-536.
 - Phadke, M.S. and Kedem, G. (1978). Computation of the exact likelihood function of multivariate moving average models, Biometrika, 65, 3, 511-519.
 - Phillips, A.W. (1966). The estimation of systems of difference equations with moving average disturbances, Econometric Society Meeting, San Francisco, reprinted in A.E. Bergstrom, et al., eds., Stability and Inflation, New York: Wiley.
 - Pierce, D.A. (1971). Distribution of residual autocorrelations in the regression model with autoregressive-moving average errors, Journal of the Royal Statistical Society, series B, 33, 140-146.
 - Pindyck, R.S. and Rubinfeld, D.L. (1981). Econometric models and economic forecasts. New York: McGraw-Hill.
 - Pollock, D.S.G. (1979). The algebra of econometrics, New York: Wiley.
 - Pukkila, T.M. (1982). On the identification of ARMA(p,q)models, Time Series Analysis: Theory and pracrice I, Amsterdam: North-Holland publishing company, 81-103.
 - Trivedi, P.L. (1970). Inventory Behavior in U.K. Manufacturing, 1956-67, Review of Economic Studies, 37, 517-527.
 - Wallis, K.F. (1972). Testing for fourth-order autocorrelation in quarterly regression equations, *Econometrica*, 40, 617-636.
 - Watson, G.S. (1955). Serial correlation in regression analysis I, Biometrika, 42, 327-341.
 - Watson, G.S. and Hannan, E.J. (1956). Serial correlation in regression analysis II, Biometrika, 43, 436-445.
 - Wise, J. (1955). Autocorrelation function and the spectral density function, Biometrika, 42, 151-159.